



ON-SITE HYDROLOGY STUDY

For

**AP Investors Group LLC
APN 0463-241-02 & 03
Apple Valley, CA**

February 22, 2023

Prepared by:

Merrell-Johnson Companies

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Job No. 3675.007

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SECTION 1

DISCUSSION

INTRODUCTION

The purpose of this study was to determine the impact, if any, of the 100-year on-site storm runoff flow on the project site as delineated on the map contained in this study. The project site encompasses approximately 72 acres of property located on the east side of Central Road, between Johnson Road to the north and Lafayette Street on the south in the northeastern area of the Town of Apple Valley, San Bernardino County, California. Development of the site will be a proposed distribution warehouse facility.

METHODOLOGY

The method in determining these peak on-site runoff flows was the unit hydrograph method as specified in the 1986 San Bernardino County Hydrology Manual and the 2010 San Bernardino County Hydrology Manual Addendum for Arid Regions. The existing on-site flow was examined and delineated from U.S.G.S. Map: Apple Valley North and an examination of the project site.

Point rainfalls for the 100-year storm were obtained from the NOAA Atlas 14 per the 2010 Addendum to the County Hydrology Manual. The 100-year 1-hour point rainfall for the site is 1.07". Per the aforementioned addendum, AMC II was used for the project site and the soil types were determined to be Soil Type A in the eastern tributary area and Soil Type C southeastern tributary area per the Natural Resources Conservation Service's "Web Soil Survey". Rainfall and maps are included as exhibits in Section 3 of this report.

The on-site flow areas examined in this study is shown in Table A.

Table A

Sub-area	Elevation Difference (ft.)	Length (ft)	Area (Ac)	Avg. Slope (ft/ft)
On-site Undeveloped	38	2,668	72.5	0.0142
On-site Developed	39	3,482	72.5	0.0112

EXISTING CONDITIONS

The site is located along the east side of Central Road between Johnson Road to the north and Lafayette Street to the south in the Town of Apple Valley, California. The property is currently vacant, undeveloped land. Central Road is a paved road with dirt shoulders. Johnson Road and Lafayette Street area both graded, unimproved roads.

The results of the offsite flow analysis are summarized in Table B.

Table B

Sub-Area	Q₁₀₀ (cfs)
On-site Undeveloped	207.7
On-site Developed	249.4

CONCLUSIONS AND RECOMMENDATIONS

During our field investigation of the site, we observed the existing conditions as stated previously. Future development of the project is being performed in conjunction with engineered improvement plans. Off-site flows were examined and delineated in the off-site hydrology study for this project. Off-site flows from the east and southeast will be intercepted along the easterly property boundary, conveyed through the project, around the proposed building and outlet along the westerly and southerly boundaries following their historical flow locations. The Apple Valley MPD flow will be intercepted as it enters the property along the northern boundary, conveyed around the proposed development and released within its historical flow location along Central Road.

On-site runoff flows will be routed through the site and intercepted in an on-site storm drain system and routed to two underground retention systems at the southeastern parking area and along the western project boundary as indicated on the map in this study and allowed to infiltrate. The proposed retention volume of these two systems is approximately 195,797 cubic feet. Overflow runoff from these systems will be routed to the storm runoff basin at the southwest corner of the project site. Excess runoff from larger storm events will outlet from this basin as weir flow across Central Road following the historical drainage patterns.

SECTION 2

EXHIBITS

VICINITY MAP

Uncommon Development

Building 1

Legend

 3675.004

Quarry Rd

Central Rd

Central Rd

Central Rd

PROJECT SITE

Google Earth

5000 ft

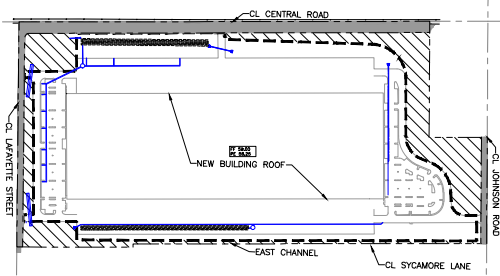


PROPOSED DEVELOPMENT PLAN

SITE MAP 1

DESCRIPTIONS AS SHOWN IN WQMP FORM 1-1

TOTAL PROPERTY:	3,159,417 SQ.FT.	72.53 ACRES
ROAD IMPROVEMENTS:	209,426 SQ.FT.	4.81 ACRES
DIVERSION AREAS:	458,902 SQ.FT.	10.53 ACRES
WQMP AREA:	2,491,089 SQ.FT.	57.19 ACRES



SITE MAP 2

DESCRIPTIONS AS SHOWN IN WQMP COMPARATIVE BREAKDOWN FORM 4.2-1(A) AND IN FORMS LISTED:

DA 1 WEST INCLUDES NORTH AND SOUTH PARKING AND WEST LOADING

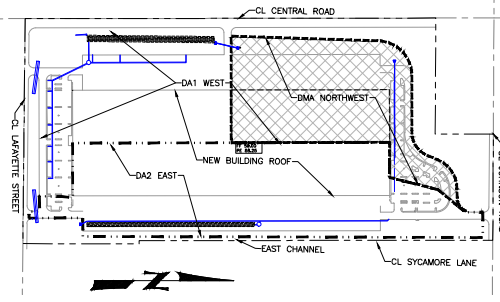
WEST DA AREA:	1,380,173 SQ.FT.	31.66 ACRES
ROOF AREA:	540,000 SQ. FT.	12.40 ACRES
IMPERVIOUS SURFACE:	601,509 SQ. FT.	13.81 ACRES
CURB LANDSCAPE:	37,721 SQ. FT.	0.87 ACRES
BIORETENTION SURFACE:	61,221 SQ. FT.	1.41 ACRES
NW PRETREATMENT SWALE:	94,447 SQ. FT.	2.17 ACRES
SW PRETREATMENT VORTEX SEPARATOR:	45,275 SQ. FT.	1.04 ACRES
PERVIOUS GRAVEL:	45,275 SQ. FT.	1.04 ACRES
U/G HORIZONTAL PERFORATED INFILTRATION PIPES:		

DESCRIPTIONS AS SHOWN IN WQMP FORM 4.3-2, ITEM #5

NORTHWEST DMA AREA:	670,290 SQ.FT.	15.39 ACRES	4.3-2 ITEM#2
ROOF AREA:	269,045 SQ. FT.	6.18 ACRES	4.3-2 ITEM#2
IMPERVIOUS SURFACE:	286,101 SQ. FT.	6.57 ACRES	4.3-2 ITEM#2
NW PRETREATMENT SWALE:	94,447 SQ. FT.	2.17 ACRES	

DA2 EAST INCLUDES EAST LOADING

EAST DA AREA:	1,110,918 SQ.FT.	25.50 ACRES	4.2-1(A) EAST
ROOF AREA:	340,000 SQ. FT.	7.78 ACRES	
IMPERVIOUS SURFACE:	440,950 SQ. FT.	10.12 ACRES	
CURB LANDSCAPE:	15,453 SQ. FT.	0.35 ACRES	
PERVIOUS GRAVEL:	114,513 SQ. FT.	2.63 ACRES	
E PRETREATMENT VORTEX SEPARATOR:			
U/G HORIZONTAL PERFORATED INFILTRATION PIPES:			



ONSITE RUNOFF FLOW PATHS

LEGEND:

- DS DOWNSPOUT LOCATION
- INLET STORM DRAIN INLET
- PRE- PRETREATMENT SYSTEM
- BMP DETENTION/INFILTRATION BMP
- TC-# BMP REFERENCE
- ROOF AREA: 1,080,000 SQ. FT.
- CONCRETE AREA HATCH TOTAL IMPERVIOUS SURFACE AREA: 1,042,459 SQ. FT.
- LANDSCAPED CURBED: 53,174 SQ.FT.
- SURFACE BASIN LANDSCAPED AREA: 56,812 SQ. FT. U/G PIPE INFILTRATION BOTTOM SURFACE: 27,919 SQ. FT.
- NATIVE SOILS GRADED TO SLOPE: 254,234 SQ.FT. GRAVEL OVER NATIVE (USES THE SAME) AS PRE DEVELOPED AS SHOWN IN FORM 4.2-3

DIVERSION METHOD, NOT A PART OF WQMP, DOES NOT COMMINGLE WITH ONSITE ACTIVITIES

DIVERSION METHOD, PIPE UNDER DRIVEWAY

DIVERSION METHOD, NOT A PART OF WQMP, DOES NOT COMMINGLE WITH ONSITE ACTIVITIES

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DIVERSION METHOD, NOT A PART OF WQMP, DOES NOT COMMINGLE WITH ONSITE ACTIVITIES

DIVERSION METHOD, PIPE UNDER DRIVEWAY

NOTE:

IF THIS PLAN IS NOT SIGNED AND DATED BY THE ENGINEER OF RECORD AND ALSO BY THE CITY ENGINEER OR UTILITY COMPANY OFFICIAL IN THE APPROVAL BLOCKS OF THIS PLAN THEN THIS PLAN IS PRELIMINARY AND NOT FOR CONSTRUCTION.

BENCHMARK

BENCHMARK

BASIS OF BEARINGS

CALIFORNIA STATE PLANE COORDINATE SYSTEM ZONE 10 NAD 83

NO.	REVISION	DATE	BY



E. CARY PACKER R.C.E. 51752

MERRELL JOHNSON

MERRELL JOHNSON ENGINEERS, INC.
22224 S. HORNWAY #100 APPLE VALLEY, CA 91707
760.296.8000 | MERRELLJOHNSON.COM

DRAWN BY: JMC
DATE: 02/03/23
DESIGNED BY: JMC
DATE: 12/08/22
APPROVED BY: JMC
DATE: 12/08/22

TOWN OF APPLE VALLEY
ENGINEERING DEPARTMENT

REVIEWED BY: JMC
DATE: 02/03/23
NORMAN B. MILLER, TOWN ENGINEER
DATE: 02/03/23
RCE 59809, EXP. DATE: 02/03/25



AP INVESTORS GROUP LLC
WQMP EXHIBIT
CENTRAL RD & LAFAYETTE ST.
68.2 ACRES

SCALE: AS SHOWN
JOB NO.: 3675.007
SHEET: 1 OF 2



THE CONTRACTOR IS REQUIRED BY GOVERNMENT CODE 4216 CALIFORNIA ONE CALL LAW TO CALL DIG ALERT AT LEAST TWO (2) WORKING DAYS BEFORE DIGGING. CONTRACTOR IS REQUIRED BY SAME CODE TO HAND-EXPOSE TO THE POINT OF NO CONFLICT 24" ON EITHER SIDE OF THE UNDERGROUND FACILITY SO YOU CAN DETERMINE ITS EXACT LOCATION BEFORE USING POWER EQUIPMENT.

3/15/2023 10:00 AM C:\Users\jmc\OneDrive\Documents\Apple Valley\2023\23-001\23-001.dwg - Author: E. CARY PACKER, R.C.E. (1) - Merrell Johnson Companies

SECTION 3

HYDROLOGY CALCULATIONS

UNIT HYDROGRAPH CALCULATIONS

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004, Version 7.0

Study date 02/23/23

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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 5006

APPLE MGA - JOB 3675.007
ON-SITE UNDEVELOPED STORM RUNOFF
100-YEAR STORM EVENT - AMC II

Storm Event Year = 100

Antecedent Moisture Condition = 2

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

Sub-Area (Ac.)	Duration (hours)	Isohyetal (In)
Rainfall data for year 10		
72.50	1	0.60

Rainfall data for year 2
72.50 6 0.72

Rainfall data for year 2
72.50 24 1.29

Rainfall data for year 100

72.50	1	1.07

Rainfall data for year 100		
72.50	6	1.98

Rainfall data for year 100		
72.50	24	3.38

+++++

***** Area-averaged max loss rate, Fm *****

SCS curve No.(AMCII)	SCS curve NO.(AMC 2)	Area (Ac.)	Area Fraction	Fp(Fig C6) (In/Hr)	Ap (dec.)	Fm (In/Hr)
67.0	67.0	72.50	1.000	0.578	1.000	0.578

Area-averaged adjusted loss rate Fm (In/Hr) = 0.578

***** Area-Averaged low loss rate fraction, Yb *****

Area (Ac.)	Area Fract	SCS CN (AMC2)	SCS CN (AMC2)	S	Pervious Yield Fr
72.50	1.000	67.0	67.0	4.93	0.232

Area-averaged catchment yield fraction, Y = 0.232

Area-averaged low loss fraction, Yb = 0.768

+++++

Watercourse length = 2668.00(Ft.)
 Length from concentration point to centroid = 1477.00(Ft.)
 Elevation difference along watercourse = 38.00(Ft.)
 Mannings friction factor along watercourse = 0.020
 Watershed area = 72.50(Ac.)
 Catchment Lag time = 0.100 hours
 Unit interval = 5.000 minutes
 Unit interval percentage of lag time = 82.9752
 Hydrograph baseflow = 0.00(CFS)
 Average maximum watershed loss rate(Fm) = 0.578(In/Hr)
 Average low loss rate fraction (Yb) = 0.768 (decimal)
 DESERT S-Graph Selected
 Computed peak 5-minute rainfall = 0.508(In)
 Computed peak 30-minute rainfall = 0.869(In)
 Specified peak 1-hour rainfall = 1.070(In)
 Computed peak 3-hour rainfall = 1.561(In)
 Specified peak 6-hour rainfall = 1.980(In)
 Specified peak 24-hour rainfall = 3.380(In)

Rainfall depth area reduction factors:

Using a total area of 72.50(Ac.) (Ref: fig. E-4)

5-minute factor = 0.997 Adjusted rainfall = 0.506(In)
 30-minute factor = 0.997 Adjusted rainfall = 0.866(In)
 1-hour factor = 0.997 Adjusted rainfall = 1.066(In)
 3-hour factor = 1.000 Adjusted rainfall = 1.560(In)
 6-hour factor = 1.000 Adjusted rainfall = 1.980(In)
 24-hour factor = 1.000 Adjusted rainfall = 3.380(In)

U n i t H y d r o g r a p h

Interval Number	'S' Graph Mean values	Unit Hydrograph (CFS)
(K = 876.80 (CFS))		
1	11.660	102.232
2	59.142	416.320
3	78.913	173.356
4	87.744	77.424
5	92.655	43.064
6	95.706	26.749
7	97.562	16.274
8	98.572	8.857
9	99.488	8.027
10	100.000	4.492

Total soil rain loss = 2.20(In)
 Total effective rainfall = 1.18(In)
Peak flow rate in flood hydrograph = 207.69(CFS)

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	75.0	150.0	225.0	300.0
0+ 5	0.0007	0.11	Q				
0+10	0.0045	0.55	Q				
0+15	0.0095	0.73	Q				
0+20	0.0151	0.81	Q				
0+25	0.0210	0.86	Q				
0+30	0.0272	0.89	Q				
0+35	0.0334	0.91	Q				
0+40	0.0398	0.92	Q				

0+45	0.0462	0.93	Q
0+50	0.0527	0.94	Q
0+55	0.0593	0.95	Q
1+ 0	0.0658	0.95	Q
1+ 5	0.0723	0.95	Q
1+10	0.0789	0.96	Q
1+15	0.0855	0.96	Q
1+20	0.0922	0.96	Q
1+25	0.0988	0.97	Q
1+30	0.1055	0.97	Q
1+35	0.1122	0.97	Q
1+40	0.1189	0.98	Q
1+45	0.1256	0.98	Q
1+50	0.1324	0.98	Q
1+55	0.1392	0.99	Q
2+ 0	0.1460	0.99	Q
2+ 5	0.1529	0.99	Q
2+10	0.1597	1.00	Q
2+15	0.1666	1.00	Q
2+20	0.1735	1.00	Q
2+25	0.1805	1.01	QV
2+30	0.1874	1.01	QV
2+35	0.1944	1.02	QV
2+40	0.2014	1.02	QV
2+45	0.2085	1.02	QV
2+50	0.2156	1.03	QV
2+55	0.2227	1.03	QV
3+ 0	0.2298	1.04	QV
3+ 5	0.2369	1.04	QV
3+10	0.2441	1.04	QV
3+15	0.2513	1.05	QV
3+20	0.2586	1.05	QV
3+25	0.2659	1.06	QV
3+30	0.2732	1.06	QV
3+35	0.2805	1.06	QV
3+40	0.2878	1.07	QV
3+45	0.2952	1.07	QV
3+50	0.3026	1.08	QV
3+55	0.3101	1.08	QV
4+ 0	0.3176	1.09	QV
4+ 5	0.3251	1.09	QV
4+10	0.3326	1.10	QV
4+15	0.3402	1.10	QV
4+20	0.3478	1.10	QV
4+25	0.3555	1.11	QV
4+30	0.3631	1.11	Q V
4+35	0.3708	1.12	Q V
4+40	0.3786	1.12	Q V
4+45	0.3864	1.13	Q V
4+50	0.3942	1.13	Q V

4+55	0.4020	1.14	Q	V
5+ 0	0.4099	1.14	Q	V
5+ 5	0.4178	1.15	Q	V
5+10	0.4258	1.16	Q	V
5+15	0.4338	1.16	Q	V
5+20	0.4418	1.17	Q	V
5+25	0.4499	1.17	Q	V
5+30	0.4580	1.18	Q	V
5+35	0.4661	1.18	Q	V
5+40	0.4743	1.19	Q	V
5+45	0.4825	1.19	Q	V
5+50	0.4908	1.20	Q	V
5+55	0.4991	1.21	Q	V
6+ 0	0.5075	1.21	Q	V
6+ 5	0.5158	1.22	Q	V
6+10	0.5243	1.22	Q	V
6+15	0.5328	1.23	Q	V
6+20	0.5413	1.24	Q	V
6+25	0.5498	1.24	Q	V
6+30	0.5585	1.25	Q	V
6+35	0.5671	1.26	Q	V
6+40	0.5758	1.26	Q	V
6+45	0.5846	1.27	Q	V
6+50	0.5934	1.28	Q	V
6+55	0.6022	1.28	Q	V
7+ 0	0.6111	1.29	Q	V
7+ 5	0.6200	1.30	Q	V
7+10	0.6290	1.31	Q	V
7+15	0.6381	1.31	Q	V
7+20	0.6472	1.32	Q	V
7+25	0.6563	1.33	Q	V
7+30	0.6655	1.34	Q	V
7+35	0.6748	1.34	Q	V
7+40	0.6841	1.35	Q	V
7+45	0.6935	1.36	Q	V
7+50	0.7029	1.37	Q	V
7+55	0.7124	1.38	Q	V
8+ 0	0.7219	1.39	Q	V
8+ 5	0.7315	1.39	Q	V
8+10	0.7412	1.40	Q	V
8+15	0.7509	1.41	Q	V
8+20	0.7607	1.42	Q	V
8+25	0.7706	1.43	Q	V
8+30	0.7805	1.44	Q	V
8+35	0.7905	1.45	Q	V
8+40	0.8005	1.46	Q	V
8+45	0.8107	1.47	Q	V
8+50	0.8208	1.48	Q	V
8+55	0.8311	1.49	Q	V
9+ 0	0.8414	1.50	Q	V

9+ 5	0.8519	1.51	Q	V
9+10	0.8623	1.52	Q	V
9+15	0.8729	1.53	Q	V
9+20	0.8835	1.55	Q	V
9+25	0.8943	1.56	Q	V
9+30	0.9051	1.57	Q	V
9+35	0.9160	1.58	Q	V
9+40	0.9269	1.59	Q	V
9+45	0.9380	1.61	Q	V
9+50	0.9491	1.62	Q	V
9+55	0.9604	1.63	Q	V
10+ 0	0.9717	1.65	Q	V
10+ 5	0.9831	1.66	Q	V
10+10	0.9946	1.67	Q	V
10+15	1.0062	1.69	Q	V
10+20	1.0180	1.70	Q	V
10+25	1.0298	1.72	Q	V
10+30	1.0417	1.73	Q	V
10+35	1.0537	1.75	Q	V
10+40	1.0659	1.76	Q	V
10+45	1.0782	1.78	Q	V
10+50	1.0905	1.80	Q	V
10+55	1.1030	1.81	Q	V
11+ 0	1.1156	1.83	Q	V
11+ 5	1.1284	1.85	Q	V
11+10	1.1413	1.87	Q	V
11+15	1.1543	1.89	Q	V
11+20	1.1674	1.91	Q	V
11+25	1.1807	1.93	Q	V
11+30	1.1941	1.95	Q	V
11+35	1.2077	1.97	Q	V
11+40	1.2214	1.99	Q	V
11+45	1.2353	2.01	Q	V
11+50	1.2493	2.04	Q	V
11+55	1.2635	2.06	Q	V
12+ 0	1.2779	2.09	Q	V
12+ 5	1.2923	2.09	Q	V
12+10	1.3061	2.00	Q	V
12+15	1.3197	1.98	Q	V
12+20	1.3334	1.99	Q	V
12+25	1.3472	2.00	Q	V
12+30	1.3612	2.03	Q	V
12+35	1.3753	2.05	Q	V
12+40	1.3896	2.08	Q	V
12+45	1.4042	2.11	Q	V
12+50	1.4190	2.15	Q	V
12+55	1.4340	2.18	Q	V
13+ 0	1.4493	2.22	Q	V
13+ 5	1.4648	2.25	Q	V
13+10	1.4806	2.30	Q	V

13+15	1.4967	2.34	Q	V				
13+20	1.5131	2.38	Q	V				
13+25	1.5299	2.43	Q	V				
13+30	1.5469	2.48	Q	V				
13+35	1.5644	2.53	Q	V				
13+40	1.5822	2.59	Q	V				
13+45	1.6003	2.64	Q	V				
13+50	1.6190	2.70	Q	V				
13+55	1.6380	2.76	Q	V				
14+ 0	1.6575	2.84	Q	V				
14+ 5	1.6775	2.91	Q	V				
14+10	1.6982	3.00	Q	V				
14+15	1.7194	3.08	Q	V				
14+20	1.7413	3.18	Q	V				
14+25	1.7638	3.27	Q	V				
14+30	1.7871	3.38	Q	V				
14+35	1.8111	3.48	Q	V				
14+40	1.8360	3.62	Q	V				
14+45	1.8618	3.74	Q	V				
14+50	1.8886	3.90	Q	V				
14+55	1.9165	4.05	Q	V				
15+ 0	1.9458	4.25	Q	V				
15+ 5	1.9764	4.44	Q	V				
15+10	2.0086	4.69	Q	V				
15+15	2.0426	4.93	Q	V				
15+20	2.0789	5.26	Q	V				
15+25	2.1167	5.50	Q	V				
15+30	2.1551	5.56	Q	V				
15+35	2.1955	5.87	Q	V				
15+40	2.2402	6.49	Q	V				
15+45	2.2900	7.23	Q	V				
15+50	2.3486	8.50	Q	V				
15+55	2.4292	11.71	Q	V				
16+ 0	2.5966	24.30	Q	V				
16+ 5	3.1680	82.96		Q	V			
16+10	4.5983	207.69				V Q		
16+15	5.2461	94.06		Q		V		
16+20	5.5699	47.01		Q		V		
16+25	5.7688	28.88	Q			V		
16+30	5.9063	19.96	Q			V		
16+35	6.0029	14.02	Q			V		
16+40	6.0709	9.89	Q			V		
16+45	6.1305	8.65	Q			V		
16+50	6.1744	6.37	Q			V		
16+55	6.2019	3.99	Q			V		
17+ 0	6.2271	3.67	Q			V		
17+ 5	6.2506	3.41	Q			V		
17+10	6.2726	3.19	Q			V		
17+15	6.2934	3.01	Q			V		
17+20	6.3130	2.85	Q			V		

17+25	6.3317	2.71	Q				V
17+30	6.3495	2.59	Q				V
17+35	6.3667	2.48	Q				V
17+40	6.3831	2.39	Q				V
17+45	6.3989	2.30	Q				V
17+50	6.4142	2.22	Q				V
17+55	6.4290	2.15	Q				V
18+ 0	6.4433	2.08	Q				V
18+ 5	6.4574	2.05	Q				V
18+10	6.4719	2.10	Q				V
18+15	6.4863	2.09	Q				V
18+20	6.5005	2.06	Q				V
18+25	6.5144	2.02	Q				V
18+30	6.5280	1.98	Q				V
18+35	6.5414	1.94	Q				V
18+40	6.5545	1.90	Q				V
18+45	6.5674	1.87	Q				V
18+50	6.5800	1.83	Q				V
18+55	6.5924	1.80	Q				V
19+ 0	6.6045	1.76	Q				V
19+ 5	6.6164	1.73	Q				V
19+10	6.6281	1.70	Q				V
19+15	6.6397	1.67	Q				V
19+20	6.6510	1.64	Q				V
19+25	6.6621	1.62	Q				V
19+30	6.6731	1.59	Q				V
19+35	6.6839	1.57	Q				V
19+40	6.6945	1.54	Q				V
19+45	6.7050	1.52	Q				V
19+50	6.7153	1.50	Q				V
19+55	6.7255	1.48	Q				V
20+ 0	6.7356	1.46	Q				V
20+ 5	6.7455	1.44	Q				V
20+10	6.7553	1.42	Q				V
20+15	6.7649	1.40	Q				V
20+20	6.7745	1.39	Q				V
20+25	6.7839	1.37	Q				V
20+30	6.7932	1.35	Q				V
20+35	6.8024	1.34	Q				V
20+40	6.8115	1.32	Q				V
20+45	6.8205	1.31	Q				V
20+50	6.8294	1.29	Q				V
20+55	6.8382	1.28	Q				V
21+ 0	6.8469	1.26	Q				V
21+ 5	6.8555	1.25	Q				V
21+10	6.8640	1.24	Q				V
21+15	6.8724	1.22	Q				V
21+20	6.8808	1.21	Q				V
21+25	6.8890	1.20	Q				V
21+30	6.8972	1.19	Q				V

21+35	6.9053	1.18	Q				V
21+40	6.9133	1.17	Q				V
21+45	6.9213	1.15	Q				V
21+50	6.9292	1.14	Q				V
21+55	6.9370	1.13	Q				V
22+ 0	6.9447	1.12	Q				V
22+ 5	6.9524	1.11	Q				V
22+10	6.9600	1.10	Q				V
22+15	6.9675	1.09	Q				V
22+20	6.9750	1.09	Q				V
22+25	6.9824	1.08	Q				V
22+30	6.9898	1.07	Q				V
22+35	6.9971	1.06	Q				V
22+40	7.0043	1.05	Q				V
22+45	7.0115	1.04	Q				V
22+50	7.0186	1.03	Q				V
22+55	7.0257	1.03	Q				V
23+ 0	7.0327	1.02	Q				V
23+ 5	7.0397	1.01	Q				V
23+10	7.0466	1.00	Q				V
23+15	7.0535	1.00	Q				V
23+20	7.0603	0.99	Q				V
23+25	7.0670	0.98	Q				V
23+30	7.0737	0.98	Q				V
23+35	7.0804	0.97	Q				V
23+40	7.0870	0.96	Q				V
23+45	7.0936	0.96	Q				V
23+50	7.1002	0.95	Q				V
23+55	7.1066	0.94	Q				V
24+ 0	7.1131	0.94	Q				V
24+ 5	7.1188	0.82	Q				V
24+10	7.1214	0.38	Q				V
24+15	7.1227	0.20	Q				V
24+20	7.1235	0.11	Q				V
24+25	7.1240	0.07	Q				V
24+30	7.1243	0.04	Q				V
24+35	7.1244	0.02	Q				V
24+40	7.1245	0.01	Q				V
24+45	7.1246	0.00	Q				V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 02/23/23

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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 5006

APPLE MGA - JOB 3675.007
ON-SITE DEVELOPED STORM RUNOFF
100-YEAR STORM EVENT - AMC II

Storm Event Year = 100

Antecedent Moisture Condition = 2

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

Sub-Area (Ac.)	Duration (hours)	Isohyetal (In)
Rainfall data for year 10		
72.50	1	0.60

Rainfall data for year 2
72.50 6 0.75

Rainfall data for year 2
72.50 24 1.29

Rainfall data for year 100

72.50	1	1.07

Rainfall data for year 100		
72.50	6	1.98

Rainfall data for year 100		
72.50	24	3.38

+++++

***** Area-averaged max loss rate, Fm *****

SCS curve No.(AMCII)	SCS curve NO.(AMC 2)	Area (Ac.)	Area Fraction	Fp(Fig C6) (In/Hr)	Ap (dec.)	Fm (In/Hr)
32.0	32.0	72.50	1.000	0.978	0.100	0.098

Area-averaged adjusted loss rate Fm (In/Hr) = 0.098

***** Area-Averaged low loss rate fraction, Yb *****

Area (Ac.)	Area Fract	SCS CN (AMC2)	SCS CN (AMC2)	S	Pervious Yield Fr
7.25	0.100	32.0	32.0	16.90	0.000
65.25	0.900	98.0	98.0	0.20	0.931

Area-averaged catchment yield fraction, Y = 0.838

Area-averaged low loss fraction, Yb = 0.162

+++++

Watercourse length = 3482.00(Ft.)
 Length from concentration point to centroid = 1400.00(Ft.)
 Elevation difference along watercourse = 39.00(Ft.)
 Mannings friction factor along watercourse = 0.015
 Watershed area = 72.50(Ac.)
 Catchment Lag time = 0.085 hours
 Unit interval = 5.000 minutes
 Unit interval percentage of lag time = 97.4877
 Hydrograph baseflow = 0.00(CFS)
 Average maximum watershed loss rate(Fm) = 0.098(In/Hr)
 Average low loss rate fraction (Yb) = 0.162 (decimal)
 DESERT S-Graph Selected
 Computed peak 5-minute rainfall = 0.508(In)
 Computed peak 30-minute rainfall = 0.869(In)
 Specified peak 1-hour rainfall = 1.070(In)
 Computed peak 3-hour rainfall = 1.561(In)
 Specified peak 6-hour rainfall = 1.980(In)
 Specified peak 24-hour rainfall = 3.380(In)

Rainfall depth area reduction factors:

Using a total area of 72.50(Ac.) (Ref: fig. E-4)

5-minute factor = 0.997	Adjusted rainfall = 0.506(In)
30-minute factor = 0.997	Adjusted rainfall = 0.866(In)
1-hour factor = 0.997	Adjusted rainfall = 1.066(In)
3-hour factor = 1.000	Adjusted rainfall = 1.560(In)
6-hour factor = 1.000	Adjusted rainfall = 1.980(In)
24-hour factor = 1.000	Adjusted rainfall = 3.380(In)

U n i t H y d r o g r a p h

+++++		
Interval	'S' Graph	Unit Hydrograph
Number	Mean values	((CFS))

	(K =	876.80 (CFS))
1	16.414	143.917
2	66.154	436.116
3	83.370	150.953
4	91.010	66.987
5	95.153	36.325
6	97.495	20.533
7	98.706	10.623
8	99.686	8.586
9	100.000	2.757

Total soil rain loss = 0.46(In)
 Total effective rainfall = 2.92(In)
Peak flow rate in flood hydrograph = 249.42(CFS)

24 - H O U R S T O R M
 R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	75.0	150.0	225.0	300.0

0+ 5	0.0038	0.55	Q				
0+10	0.0189	2.20	Q				
0+15	0.0381	2.78	Q				
0+20	0.0591	3.05	Q				
0+25	0.0811	3.19	Q				
0+30	0.1037	3.28	Q				
0+35	0.1267	3.33	Q				
0+40	0.1499	3.38	Q				

0+45	0.1734	3.40	Q
0+50	0.1969	3.41	Q
0+55	0.2204	3.42	Q
1+ 0	0.2441	3.43	Q
1+ 5	0.2678	3.45	Q
1+10	0.2916	3.46	Q
1+15	0.3155	3.47	Q
1+20	0.3395	3.48	Q
1+25	0.3635	3.49	Q
1+30	0.3877	3.51	Q
1+35	0.4119	3.52	Q
1+40	0.4362	3.53	Q
1+45	0.4606	3.54	QV
1+50	0.4851	3.56	QV
1+55	0.5096	3.57	QV
2+ 0	0.5343	3.58	QV
2+ 5	0.5591	3.59	QV
2+10	0.5839	3.61	QV
2+15	0.6088	3.62	QV
2+20	0.6338	3.63	QV
2+25	0.6590	3.65	QV
2+30	0.6842	3.66	QV
2+35	0.7095	3.67	QV
2+40	0.7349	3.69	QV
2+45	0.7604	3.70	QV
2+50	0.7860	3.72	QV
2+55	0.8116	3.73	QV
3+ 0	0.8374	3.75	QV
3+ 5	0.8633	3.76	QV
3+10	0.8893	3.77	Q V
3+15	0.9154	3.79	Q V
3+20	0.9416	3.80	Q V
3+25	0.9679	3.82	Q V
3+30	0.9943	3.84	Q V
3+35	1.0208	3.85	Q V
3+40	1.0475	3.87	Q V
3+45	1.0742	3.88	Q V
3+50	1.1010	3.90	Q V
3+55	1.1280	3.91	Q V
4+ 0	1.1551	3.93	Q V
4+ 5	1.1822	3.95	Q V
4+10	1.2096	3.96	Q V
4+15	1.2370	3.98	Q V
4+20	1.2645	4.00	Q V
4+25	1.2922	4.01	Q V
4+30	1.3199	4.03	Q V
4+35	1.3478	4.05	Q V
4+40	1.3758	4.07	Q V
4+45	1.4040	4.09	Q V
4+50	1.4323	4.11	Q V

4+55	1.4607	4.12	Q	V
5+ 0	1.4892	4.14	Q	V
5+ 5	1.5178	4.16	Q	V
5+10	1.5466	4.18	Q	V
5+15	1.5756	4.20	Q	V
5+20	1.6046	4.22	Q	V
5+25	1.6338	4.24	Q	V
5+30	1.6632	4.26	Q	V
5+35	1.6927	4.28	Q	V
5+40	1.7223	4.30	Q	V
5+45	1.7521	4.32	Q	V
5+50	1.7820	4.34	Q	V
5+55	1.8120	4.36	Q	V
6+ 0	1.8423	4.39	Q	V
6+ 5	1.8726	4.41	Q	V
6+10	1.9032	4.43	Q	V
6+15	1.9338	4.45	Q	V
6+20	1.9647	4.48	Q	V
6+25	1.9957	4.50	Q	V
6+30	2.0269	4.53	Q	V
6+35	2.0582	4.55	Q	V
6+40	2.0897	4.57	Q	V
6+45	2.1213	4.60	Q	V
6+50	2.1532	4.62	Q	V
6+55	2.1852	4.65	Q	V
7+ 0	2.2174	4.68	Q	V
7+ 5	2.2498	4.70	Q	V
7+10	2.2823	4.73	Q	V
7+15	2.3151	4.75	Q	V
7+20	2.3480	4.78	Q	V
7+25	2.3811	4.81	Q	V
7+30	2.4145	4.84	Q	V
7+35	2.4480	4.87	Q	V
7+40	2.4817	4.90	Q	V
7+45	2.5156	4.92	Q	V
7+50	2.5498	4.96	Q	V
7+55	2.5841	4.99	Q	V
8+ 0	2.6187	5.02	Q	V
8+ 5	2.6534	5.05	Q	V
8+10	2.6884	5.08	Q	V
8+15	2.7236	5.11	Q	V
8+20	2.7591	5.15	Q	V
8+25	2.7948	5.18	Q	V
8+30	2.8307	5.22	Q	V
8+35	2.8668	5.25	Q	V
8+40	2.9032	5.29	Q	V
8+45	2.9399	5.32	Q	V
8+50	2.9768	5.36	Q	V
8+55	3.0140	5.40	Q	V
9+ 0	3.0514	5.44	Q	V

9+ 5	3.0891	5.47	Q	V				
9+10	3.1271	5.52	Q	V				
9+15	3.1653	5.55	Q	V				
9+20	3.2039	5.60	Q	V				
9+25	3.2427	5.64	Q	V				
9+30	3.2818	5.68	Q	V				
9+35	3.3212	5.72	Q	V				
9+40	3.3610	5.77	Q	V				
9+45	3.4010	5.81	Q	V				
9+50	3.4414	5.86	Q	V				
9+55	3.4821	5.91	Q	V				
10+ 0	3.5231	5.96	Q	V				
10+ 5	3.5645	6.01	Q	V				
10+10	3.6062	6.06	Q	V				
10+15	3.6483	6.11	Q	V				
10+20	3.6908	6.17	Q	V				
10+25	3.7336	6.22	Q	V				
10+30	3.7768	6.28	Q	V				
10+35	3.8204	6.33	Q	V				
10+40	3.8644	6.39	Q	V				
10+45	3.9088	6.45	Q	V				
10+50	3.9537	6.51	Q	V				
10+55	3.9990	6.57	Q	V				
11+ 0	4.0447	6.64	Q	V				
11+ 5	4.0909	6.70	Q	V				
11+10	4.1375	6.78	Q	V				
11+15	4.1846	6.84	Q	V				
11+20	4.2323	6.92	Q	V				
11+25	4.2804	6.99	Q	V				
11+30	4.3291	7.07	Q	V				
11+35	4.3782	7.14	Q	V				
11+40	4.4280	7.23	Q	V				
11+45	4.4783	7.30	Q	V				
11+50	4.5292	7.40	Q	V				
11+55	4.5807	7.48	Q	V				
12+ 0	4.6329	7.57	Q	V				
12+ 5	4.6847	7.52	Q	V				
12+10	4.7343	7.20	Q	V				
12+15	4.7835	7.15	Q	V				
12+20	4.8330	7.19	Q	V				
12+25	4.8829	7.25	Q	V				
12+30	4.9335	7.34	Q	V				
12+35	4.9847	7.43	Q	V				
12+40	5.0367	7.55	Q	V				
12+45	5.0894	7.66	Q	V				
12+50	5.1431	7.79	Q	V				
12+55	5.1976	7.91	Q	V				
13+ 0	5.2531	8.06	Q	V				
13+ 5	5.3094	8.19	Q	V				
13+10	5.3669	8.35	Q	V				

13+15	5.4254	8.49	Q	V			
13+20	5.4850	8.66	Q	V			
13+25	5.5458	8.82	Q	V			
13+30	5.6078	9.01	Q	V			
13+35	5.6711	9.19	Q	V			
13+40	5.7358	9.40	Q	V			
13+45	5.8019	9.59	Q	V			
13+50	5.8696	9.83	Q	V			
13+55	5.9388	10.05	Q	V			
14+ 0	6.0098	10.32	Q	V			
14+ 5	6.0827	10.58	Q	V			
14+10	6.1579	10.92	Q	V			
14+15	6.2351	11.22	Q	V			
14+20	6.3148	11.57	Q	V			
14+25	6.3968	11.90	Q	V			
14+30	6.4816	12.32	Q	V			
14+35	6.5691	12.70	Q	V			
14+40	6.6599	13.19	Q	V			
14+45	6.7539	13.65	Q	V			
14+50	6.8520	14.23	Q	V			
14+55	6.9539	14.80	Q	V			
15+ 0	7.0607	15.52	Q	V			
15+ 5	7.1725	16.23	Q	V			
15+10	7.2906	17.15	Q	V			
15+15	7.4151	18.07	Q	V			
15+20	7.5480	19.30	Q	V			
15+25	7.6862	20.07	Q	V			
15+30	7.8259	20.28	Q	V			
15+35	7.9743	21.55	Q	V			
15+40	8.1390	23.91	Q	V			
15+45	8.3239	26.85	Q	V			
15+50	8.5428	31.78	Q	V			
15+55	8.8182	39.99	Q	V			
16+ 0	9.2236	58.86	Q	V			
16+ 5	10.1579	135.67	Q	V	V		
16+10	11.8757	249.42			V	Q	
16+15	12.6732	115.80		Q	V		
16+20	13.1332	66.80		Q	V		
16+25	13.4470	45.56		Q	V		
16+30	13.6846	34.49	Q		V		
16+35	13.8682	26.67	Q		V		
16+40	14.0253	22.80	Q		V		
16+45	14.1497	18.06	Q		V		
16+50	14.2544	15.20	Q		V		
16+55	14.3502	13.91	Q		V		
17+ 0	14.4391	12.91	Q		V		
17+ 5	14.5221	12.06	Q		V		
17+10	14.6000	11.30	Q		V		
17+15	14.6735	10.68	Q		V		
17+20	14.7433	10.14	Q		V		

17+25	14.8099	9.66	Q			V
17+30	14.8735	9.24	Q			V
17+35	14.9346	8.87	Q			V
17+40	14.9934	8.53	Q			V
17+45	15.0500	8.22	Q			V
17+50	15.1047	7.94	Q			V
17+55	15.1576	7.69	Q			V
18+ 0	15.2089	7.45	Q			V
18+ 5	15.2597	7.37	Q			V
18+10	15.3120	7.59	Q			V
18+15	15.3639	7.54	Q			V
18+20	15.4149	7.42	Q			V
18+25	15.4651	7.28	Q			V
18+30	15.5142	7.13	Q			V
18+35	15.5623	6.99	Q			V
18+40	15.6095	6.85	Q			V
18+45	15.6558	6.71	Q			V
18+50	15.7011	6.58	Q			V
18+55	15.7456	6.46	Q			V
19+ 0	15.7892	6.34	Q			V
19+ 5	15.8321	6.23	Q			V
19+10	15.8742	6.12	Q			V
19+15	15.9157	6.01	Q			V
19+20	15.9564	5.92	Q			V
19+25	15.9965	5.82	Q			V
19+30	16.0360	5.73	Q			V
19+35	16.0748	5.64	Q			V
19+40	16.1131	5.56	Q			V
19+45	16.1508	5.48	Q			V
19+50	16.1880	5.40	Q			V
19+55	16.2247	5.33	Q			V
20+ 0	16.2609	5.25	Q			V
20+ 5	16.2966	5.18	Q			V
20+10	16.3319	5.12	Q			V
20+15	16.3667	5.05	Q			V
20+20	16.4010	4.99	Q			V
20+25	16.4350	4.93	Q			V
20+30	16.4685	4.87	Q			V
20+35	16.5017	4.81	Q			V
20+40	16.5344	4.76	Q			V
20+45	16.5668	4.70	Q			V
20+50	16.5989	4.65	Q			V
20+55	16.6305	4.60	Q			V
21+ 0	16.6619	4.55	Q			V
21+ 5	16.6929	4.50	Q			V
21+10	16.7236	4.46	Q			V
21+15	16.7540	4.41	Q			V
21+20	16.7841	4.37	Q			V
21+25	16.8139	4.32	Q			V
21+30	16.8434	4.28	Q			V

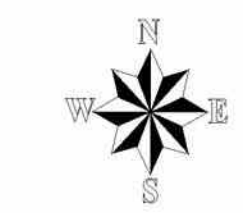
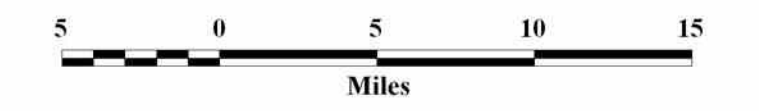
21+35	16.8726	4.24	Q				V
21+40	16.9015	4.20	Q				V
21+45	16.9302	4.16	Q				V
21+50	16.9586	4.13	Q				V
21+55	16.9868	4.09	Q				V
22+ 0	17.0147	4.05	Q				V
22+ 5	17.0423	4.02	Q				V
22+10	17.0698	3.98	Q				V
22+15	17.0969	3.95	Q				V
22+20	17.1239	3.92	Q				V
22+25	17.1507	3.88	Q				V
22+30	17.1772	3.85	Q				V
22+35	17.2035	3.82	Q				V
22+40	17.2296	3.79	Q				V
22+45	17.2555	3.76	Q				V
22+50	17.2812	3.73	Q				V
22+55	17.3067	3.70	Q				V
23+ 0	17.3320	3.68	Q				V
23+ 5	17.3571	3.65	Q				V
23+10	17.3821	3.62	Q				V
23+15	17.4068	3.59	Q				V
23+20	17.4314	3.57	Q				V
23+25	17.4558	3.54	Q				V
23+30	17.4800	3.52	Q				V
23+35	17.5041	3.49	Q				V
23+40	17.5280	3.47	Q				V
23+45	17.5517	3.45	Q				V
23+50	17.5753	3.42	Q				V
23+55	17.5987	3.40	Q				V
24+ 0	17.6220	3.38	Q				V
24+ 5	17.6414	2.81	Q				V
24+10	17.6492	1.14	Q				V
24+15	17.6531	0.56	Q				V
24+20	17.6552	0.30	Q				V
24+25	17.6563	0.16	Q				V
24+30	17.6569	0.08	Q				V
24+35	17.6572	0.04	Q				V
24+40	17.6572	0.01	Q				V

2010 ANTECEDENT MOISTURE CONDITION (AMC) MAP

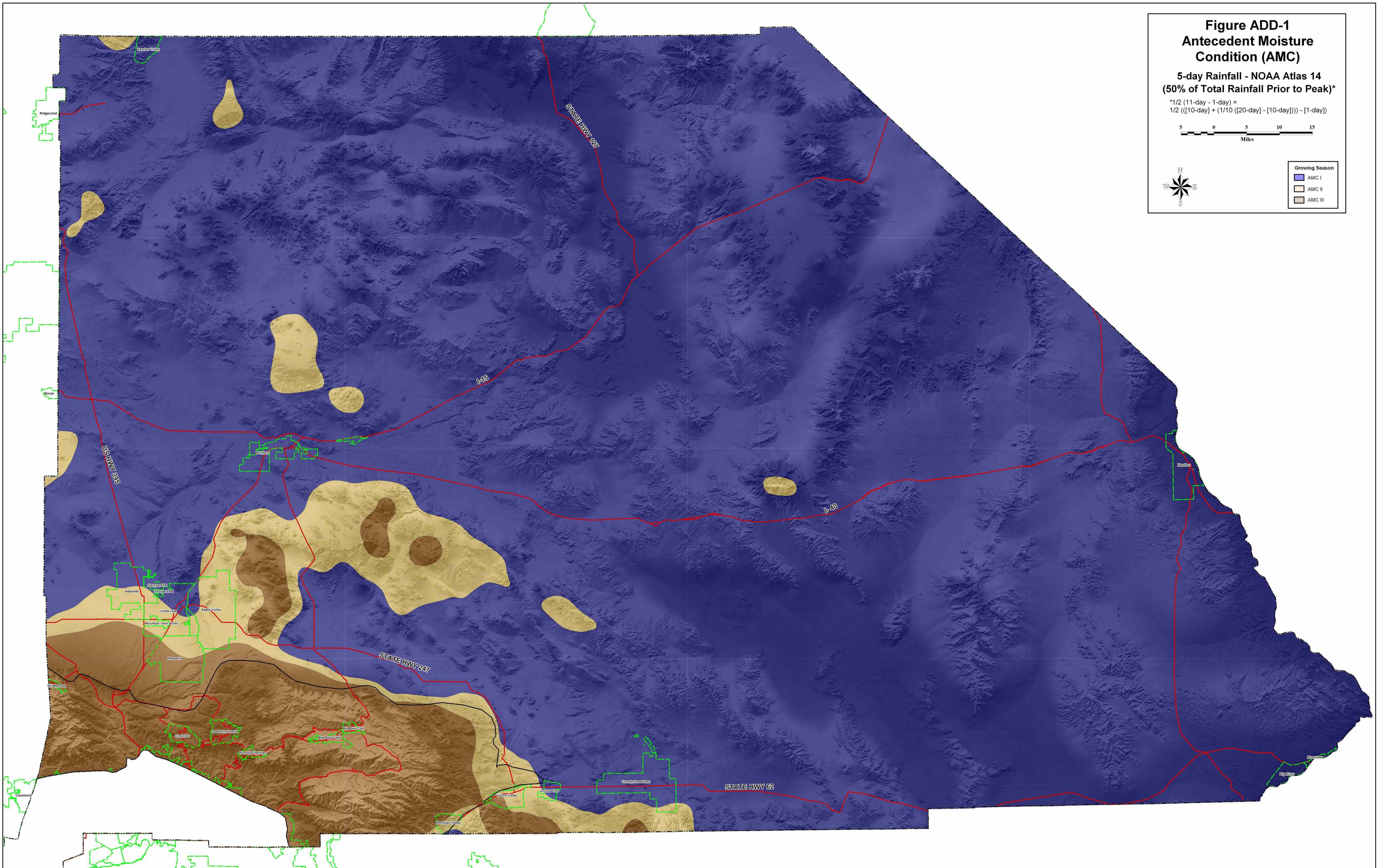
**Figure ADD-1
Antecedent Moisture
Condition (AMC)**

**5-day Rainfall - NOAA Atlas 14
(50% of Total Rainfall Prior to Peak)***

* $1/2 (11\text{-day} - 1\text{-day}) =$
 $1/2 ((10\text{-day}) + (1/10 ((20\text{-day}) - [10\text{-day}])) - [1\text{-day}])$




Growing Season	
AMC I	Dark Blue
AMC II	Light Yellow
AMC III	Dark Brown



Uncommon Development

Antecedent Moisture Condition II

Legend

 3675.004

Quarry Rd

Central Rd

Central Rd

PROJECT SITE

Google Earth

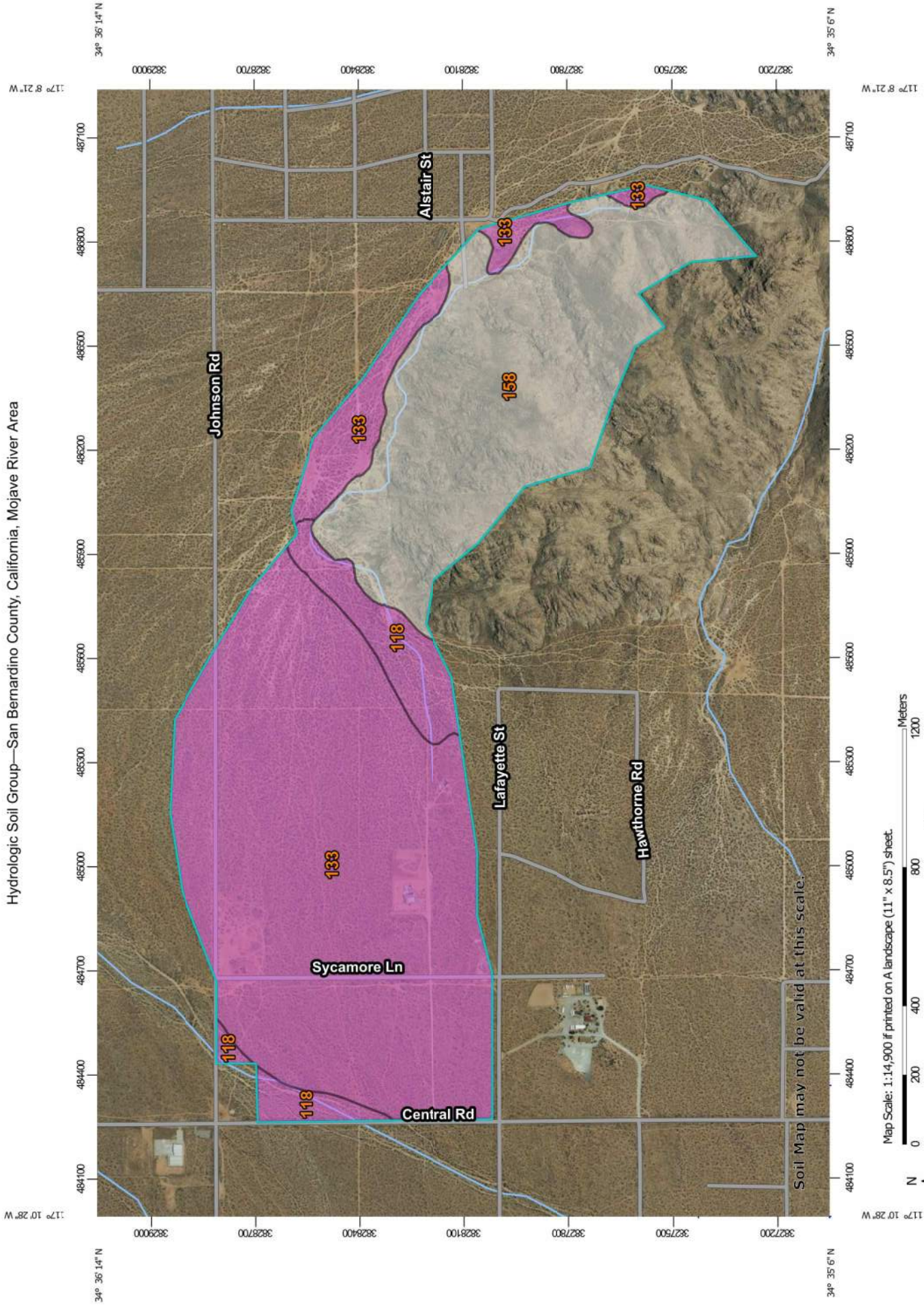


1 mi

EXHIBITS

SOILS MAP

Hydrologic Soil Group—San Bernardino County, California, Mojave River Area

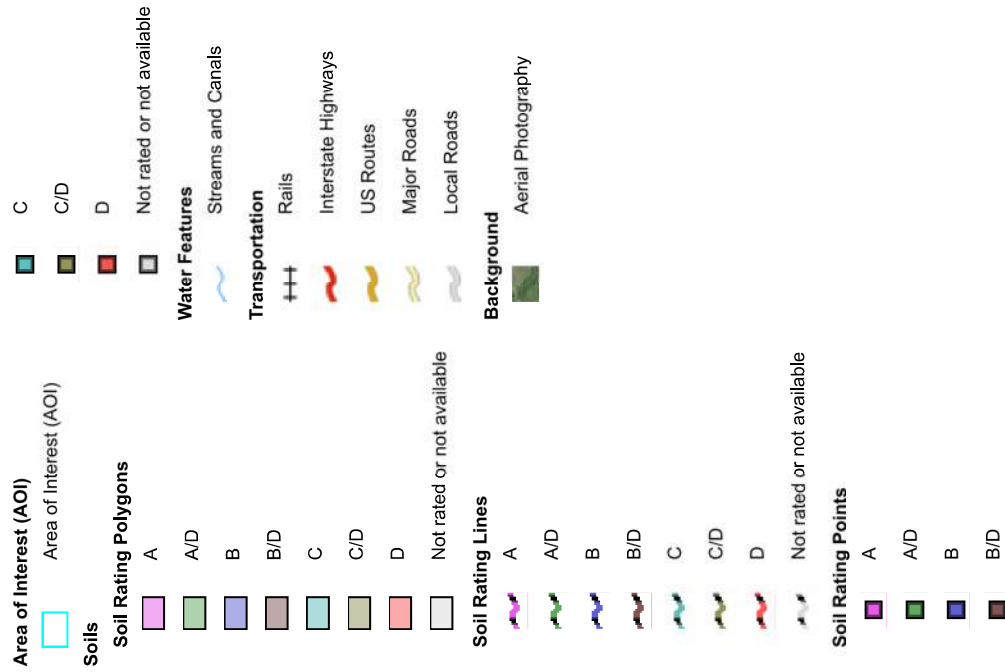


Map Scale: 1:14,900 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

MAP LEGEND



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Bernardino County, California, Mojave River Area

Survey Area Data: Version 13, Sep 13, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 27, 2021—May 24, 2021

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
118	CAJON-ARIZO COMPLEX, 2 TO 15 PERCENT SLOPES*	A	31.5	6.5%
133	HELENDALE-BRYMAN LOAMY SANDS, 2 TO 5 PERCENT SLOPES*	A	293.0	60.3%
158	ROCK OUTCROP- LITHIC TORRIORTHENTS COMPLEX, 15 TO 50 PERCENT SLOPES*		161.4	33.2%
Totals for Area of Interest			485.9	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

NOAA ATLAS 14 POINT RAINFALLS



* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF_tabular](#) | [PF_graphical](#) | [Maps_&_aerials](#)

PF tabular

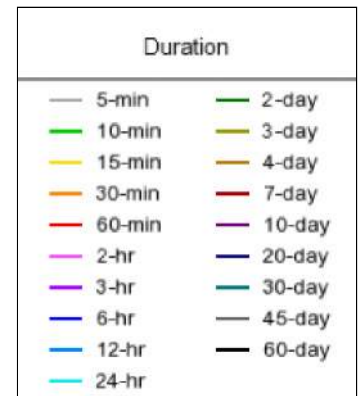
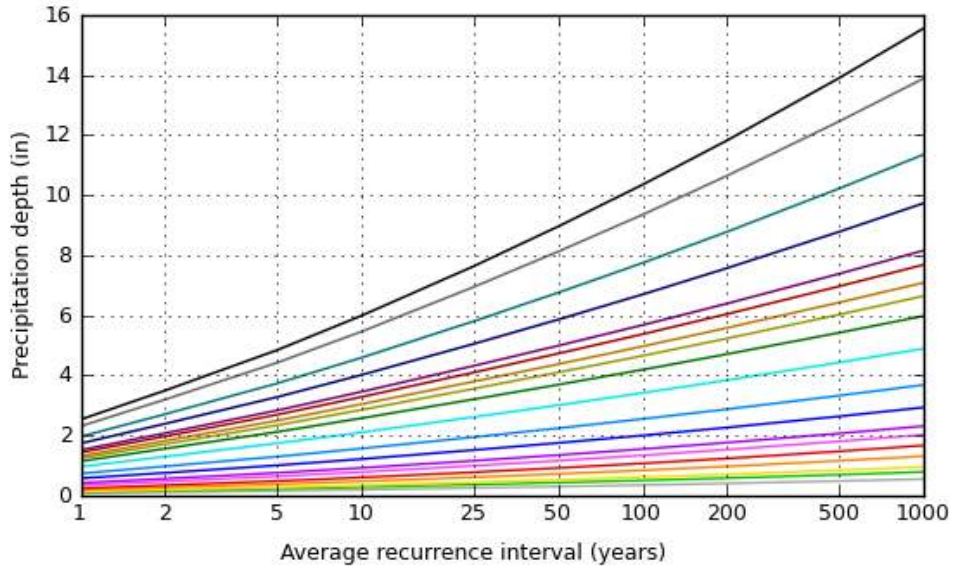
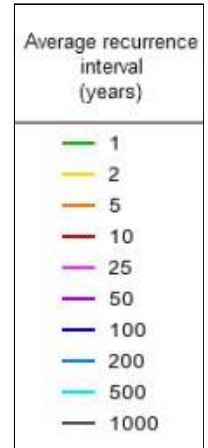
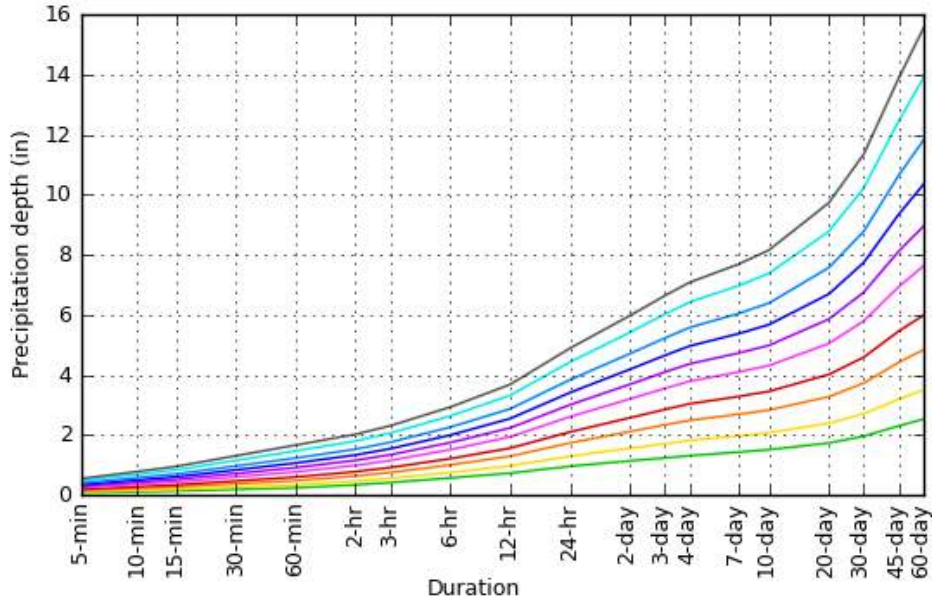
PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.082 (0.067-0.100)	0.115 (0.094-0.141)	0.161 (0.132-0.198)	0.200 (0.163-0.249)	0.258 (0.203-0.330)	0.305 (0.235-0.399)	0.355 (0.267-0.475)	0.409 (0.300-0.564)	0.487 (0.343-0.699)	0.552 (0.376-0.819)
10-min	0.117 (0.096-0.144)	0.165 (0.135-0.202)	0.230 (0.189-0.284)	0.287 (0.234-0.357)	0.369 (0.291-0.474)	0.436 (0.337-0.571)	0.508 (0.383-0.681)	0.586 (0.430-0.808)	0.698 (0.492-1.00)	0.791 (0.538-1.17)
15-min	0.142 (0.117-0.174)	0.199 (0.164-0.244)	0.279 (0.229-0.343)	0.347 (0.283-0.431)	0.447 (0.352-0.573)	0.528 (0.407-0.691)	0.615 (0.463-0.824)	0.709 (0.520-0.977)	0.845 (0.595-1.21)	0.957 (0.651-1.42)
30-min	0.195 (0.160-0.239)	0.273 (0.225-0.336)	0.383 (0.314-0.471)	0.477 (0.388-0.592)	0.613 (0.483-0.787)	0.725 (0.560-0.949)	0.844 (0.636-1.13)	0.974 (0.714-1.34)	1.16 (0.817-1.67)	1.31 (0.894-1.95)
60-min	0.248 (0.204-0.304)	0.348 (0.286-0.427)	0.487 (0.399-0.599)	0.607 (0.494-0.753)	0.780 (0.615-1.00)	0.922 (0.712-1.21)	1.07 (0.809-1.44)	1.24 (0.908-1.71)	1.48 (1.04-2.12)	1.67 (1.14-2.48)
2-hr	0.350 (0.288-0.429)	0.473 (0.389-0.580)	0.642 (0.527-0.791)	0.787 (0.640-0.977)	0.994 (0.783-1.27)	1.16 (0.897-1.52)	1.34 (1.01-1.80)	1.53 (1.12-2.11)	1.81 (1.27-2.59)	2.03 (1.38-3.01)
3-hr	0.425 (0.350-0.521)	0.566 (0.466-0.695)	0.760 (0.624-0.936)	0.925 (0.753-1.15)	1.16 (0.914-1.49)	1.35 (1.04-1.77)	1.55 (1.17-2.08)	1.77 (1.29-2.43)	2.07 (1.46-2.97)	2.32 (1.58-3.44)
6-hr	0.577 (0.475-0.707)	0.760 (0.625-0.933)	1.01 (0.828-1.24)	1.22 (0.992-1.51)	1.52 (1.20-1.95)	1.75 (1.35-2.30)	2.00 (1.51-2.68)	2.27 (1.66-3.12)	2.64 (1.86-3.79)	2.94 (2.00-4.36)
12-hr	0.738 (0.608-0.905)	0.977 (0.804-1.20)	1.30 (1.07-1.60)	1.57 (1.28-1.95)	1.95 (1.53-2.50)	2.24 (1.73-2.94)	2.55 (1.92-3.42)	2.88 (2.11-3.96)	3.33 (2.34-4.78)	3.69 (2.51-5.47)
24-hr	0.967 (0.858-1.11)	1.30 (1.15-1.50)	1.74 (1.54-2.01)	2.11 (1.85-2.46)	2.61 (2.22-3.15)	3.01 (2.50-3.70)	3.42 (2.77-4.30)	3.84 (3.03-4.98)	4.43 (3.35-5.98)	4.89 (3.57-6.84)
2-day	1.15 (1.02-1.32)	1.57 (1.39-1.80)	2.12 (1.87-2.45)	2.58 (2.26-3.00)	3.21 (2.72-3.86)	3.69 (3.07-4.54)	4.19 (3.40-5.28)	4.71 (3.71-6.10)	5.42 (4.10-7.32)	5.98 (4.37-8.35)
3-day	1.25 (1.10-1.43)	1.72 (1.52-1.98)	2.34 (2.07-2.71)	2.86 (2.50-3.33)	3.56 (3.01-4.28)	4.10 (3.40-5.04)	4.65 (3.77-5.86)	5.23 (4.12-6.78)	6.02 (4.55-8.13)	6.64 (4.85-9.28)
4-day	1.32 (1.17-1.52)	1.83 (1.62-2.10)	2.50 (2.21-2.88)	3.05 (2.67-3.55)	3.80 (3.22-4.57)	4.37 (3.63-5.38)	4.97 (4.03-6.26)	5.58 (4.40-7.23)	6.43 (4.86-8.67)	7.09 (5.18-9.90)
7-day	1.44 (1.27-1.65)	1.98 (1.75-2.28)	2.69 (2.38-3.11)	3.29 (2.88-3.83)	4.10 (3.47-4.93)	4.73 (3.92-5.81)	5.37 (4.35-6.77)	6.04 (4.76-7.83)	6.96 (5.26-9.40)	7.68 (5.61-10.7)
10-day	1.52 (1.35-1.75)	2.08 (1.84-2.40)	2.84 (2.50-3.27)	3.46 (3.03-4.03)	4.32 (3.66-5.20)	4.99 (4.14-6.13)	5.68 (4.60-7.15)	6.39 (5.04-8.28)	7.38 (5.58-9.96)	8.15 (5.96-11.4)
20-day	1.74 (1.54-2.00)	2.39 (2.12-2.76)	3.28 (2.90-3.79)	4.02 (3.52-4.68)	5.05 (4.28-6.08)	5.86 (4.86-7.20)	6.69 (5.42-8.43)	7.57 (5.97-9.81)	8.78 (6.64-11.8)	9.73 (7.11-13.6)
30-day	1.97 (1.74-2.26)	2.71 (2.40-3.13)	3.73 (3.30-4.31)	4.59 (4.02-5.35)	5.80 (4.92-6.98)	6.75 (5.61-8.30)	7.74 (6.27-9.75)	8.78 (6.92-11.4)	10.2 (7.72-13.8)	11.3 (8.29-15.9)
45-day	2.31 (2.05-2.66)	3.20 (2.83-3.69)	4.42 (3.91-5.11)	5.46 (4.79-6.36)	6.94 (5.88-8.35)	8.12 (6.74-9.98)	9.35 (7.57-11.8)	10.6 (8.39-13.8)	12.4 (9.41-16.8)	13.9 (10.1-19.4)
60-day	2.53 (2.25-2.92)	3.50 (3.10-4.03)	4.84 (4.28-5.59)	5.99 (5.25-6.97)	7.63 (6.47-9.18)	8.95 (7.43-11.0)	10.3 (8.38-13.0)	11.8 (9.31-15.3)	13.9 (10.5-18.7)	15.5 (11.4-21.7)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against average maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

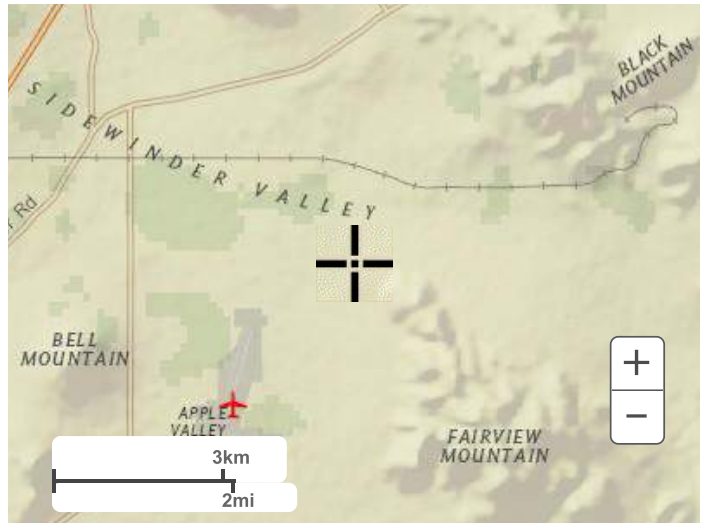
PDS-based depth-duration-frequency (DDF) curves
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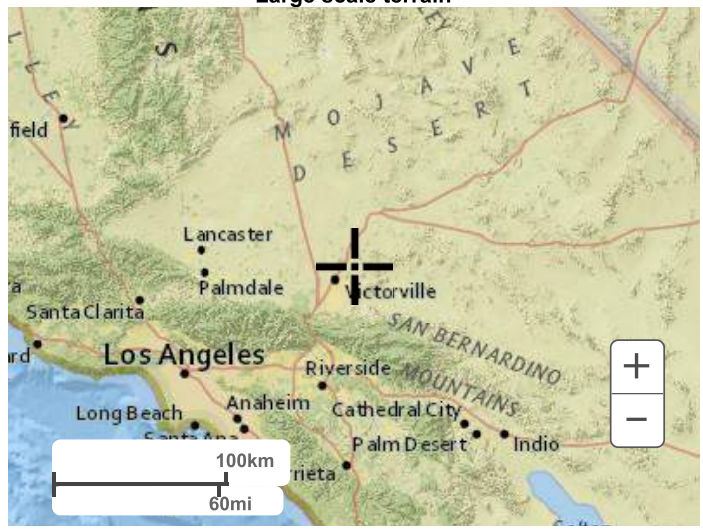
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Maps & aerials

Small scale terrain



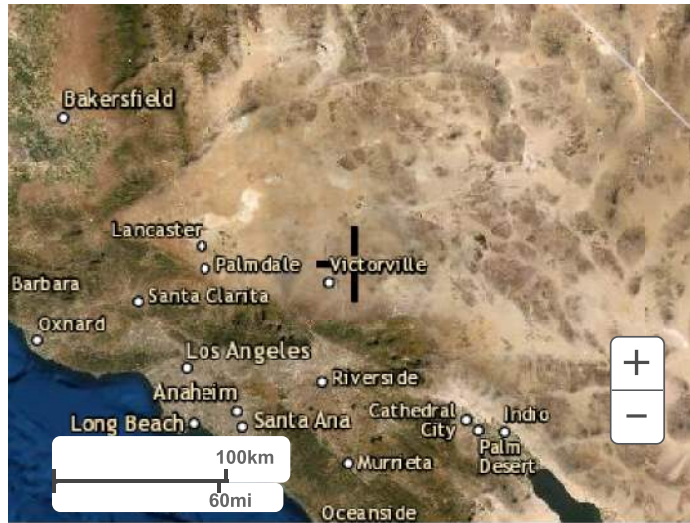
Large scale terrain



Large scale map



Large scale aerial



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