

GEOTECHNICAL INVESTIGATION REPORT

GEOTECHNICAL INVESTIGATION Proposed Industrial Warehouse NE Corner of Cardova Road and Dachshund Avenue Apple Valley, CA

Prepared for Redwood West Submitted by Merrell Johnson Geotechnical, Inc. December 1, 2023

MERRELL JOHNSON

December 1, 2023

Butterfly Equity Partners and /or RW Apple Valley II and /or Assignee, and/or Linkup, LLC 220 Newport Center Drive, Ste 11-557 Newport Beach, CA 92660

Re: Geotechnical Investigation Report | Proposed Industrial Warehouse | NE Corner of Cardova Road and Dachshund Avenue, Apple Valley, CA 92307 | M.J.G. Project No. 3813.006.500

Ladies and Gentlemen:

This letter transmits Merrell Johnson Geotechnical's Geotechnical Investigation Report for the subject industrial warehouse building. The investigation was planned and performed based on the proposed project development illustrated on the Conceptual Grading Plan prepared by Merrell Johnson, dated September 18, 2023.

We trust that the enclosed information will be useful for the design and construction phases of this project. If you have any questions, please do not hesitate to contact our firm.

Sincerely,

Merrell Johnson Companies

Brad S. Merrell, P.E., President Merrell Johnson Geotechnical, Inc. R.C.E. 49423



Jeff S. Burns, Project Manager Merrell Johnson Geotechnical, Inc.



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INTRODUCTION

Project Description

This report presents the results of the geotechnical investigation Merrell Johnson Geotechnical (MJG) performed for the new warehouse planned for the 68.2-acre parcel located on the northeast corner of Cardova and Dachshund Avenue, Apple Valley, CA. The location of the proposed development is shown on the Site Vicinity Map, Google Earth Site Image, Site Plan, and Conceptual Grading Plan, included with this report as Appendix A, Figures 1-4.

The proposed industrial warehouse will occupy a plan area of 1,346,270 square feet (SF) and includes a 26,880 SF mezzanine. Proposed site improvements will include truck loading docks, truck trailer parking, automobile parking, driveways, retention basin, utilities, and other ancillary improvements. Maximum cut and fill depths required to grade the site are anticipated to be about 15 feet and 10 feet, respectively, plus building pad overexcavation.

Proposed off-site improvements will include installing utilities and paving Dachshund Avenue from Quarry Road south to Johnson Road and Cardova Road westward from the project's southeast corner to Dale Evans Parkway.

Scope of Services

The scope of work for this project consisted of field exploration, laboratory testing, engineering analyses, and preparation of this report. The results of the field exploration and laboratory test programs were analyzed to develop conclusions and recommendations regarding:

- Subsurface conditions underlying areas to be developed
- Site preparation and grading
- Excavation conditions
- Foundation support for the new structure along with soils engineering criteria for foundation design
- Support for slab-on-grade floors
- Concrete and flexible pavement structural sections for parking and driveway/fire lanes
- Flexible pavement structural sections for Dachshund Avenue and Cardova Road off-site street improvements

FIELD EXPLORATION AND LABORATORY TESTING

Field Exploration

Subsurface conditions were explored by drilling five (5) test borings within the warehouse building limits, one (1) to a depth of 50 feet and four (4) to a depth of 25 feet. The 50-foot-deep test boring was also used to evaluate the soil liquefaction potential.

Outside the limits of the proposed warehouse, two 10-feet-deep test borings were drilled within the proposed retention basin, six 5-feet-deep test borings within the onsite loading/parking areas, and four 5-feet-deep testing borings within the off-site Cardova and Dachshund Avenue improvement areas.

The locations of the test borings are shown on Conceptual Grading Plan, Figure 3 in Appendix A. The borings were logged by an MJG's representative, who also collected samples of the materials encountered for examination and laboratory testing. Bulk samples were collected from drill cuttings. Relatively undisturbed samples were obtained by driving a 2.5-inch inside diameter modified California sampler with a 140-pound hammer falling 30 inches. Blow counts required to drive the sampler each 6 inches of an 18-inch (or less) drive are noted on the boring logs as "N" value.

Standard Penetration Tests (SPTs) were performed at selected depths by driving a 1.4-inch inside diameter sampler 18 inches with a 140-pound hammer falling 30 inches. The blow counts required to drive the sampler each 6 inches of the drive are noted on the boring logs as "N" value. Disturbed samples were collected from the SPT sampler at the time of driving.

The logs of the test borings are in Appendix B. Soils are described according to the Unified Soil Classification System explained in Appendix B.

Laboratory Testing

The laboratory program included the following tests:

- ASTM D 422 Grain Size Analysis
- ASTM D 1557 Maximum Density
- ASTM D 2419 Sand Equivalent
- ASTM D 2435 / CT-219 Consolidation of Soils
- ASTM D 2844 / CT 301 Resistance to R-value
- ASTM D 2937 In-place Moisture Content and Dry Density
- ASTM D 3080 Direct Shear
- ASTM D 4829 Expansion Index of Soil
- G51/CT643, CT417, CT422 Corrosion Potential

The results of the laboratory tests are summarized in Appendix C.

SITE AND SUBSURFACE CONDITIONS

Site Conditions

The 68.2-acre site is located on the northeast corner of Cardova and Dachshund Avenue. The property is undeveloped and covered with sparce desert vegetation. The ground surface slopes (descends) gradually towards the southwest at an inclination of about 1.5 percent. Cardova and Dachshund Avenue are unpaved. Quarry Road bounds the north side of the site. Quarry Road is a paved private road with no legal paved access to the project site.

Subsurface Conditions

The site is blanketed by medium dense silty sand (SM) to a depth of about 3 feet where it becomes dense. At a depth of about 5 feet, dense poorly graded sand with silt with some gravel and cobbles (SP-SM) was encountered and extended to the depth explored (50 feet). A boulder was encountered in Boring No. 1 at a depth of 30 feet.

Expansion Potential

Results of an expansion index test (ASTM D4829) performed on a near-surface soil sample from Boring No. 3 within the proposed warehouse limits exhibited an expansion index of 2, which corresponds to a very low expansion potential.

Geologic Setting

The subject site is located within a natural geomorphic province in southern California known as the Mojave Desert. This province consists of a broad interior region of isolated mountain ranges separated by expanses of desert plains and is characterized by the numerous interior enclosed drainages and playas. The Mojave Desert is in large, bounded structurally on the southwest by the San Andreas Fault and on the northwest by the Garlock Faults, and is ill-defined along the east where the structural patterns resemble the Basin and Range Province to the north and east. This province exhibits interior drainage, including the Mojave River, which has its source in the San Bernardino Mountains and would extend into Death Valley if there was enough water.

The geologic units of this region generally consist of three main divisions being: 1) Crystalline rocks of pre-Tertiary age; 2) sediments and volcanic rocks of Tertiary age; and 3) sediments and basalt flows of Quaternary age. Regionally, the site is located along a large alluvial plain, locally underlain by Quaternary age alluvium and older that has been derived predominantly as outwash from the adjacent highlands to the north and east along Sidewinder Valley. These sediments are believed to be less than 500± feet locally (Subsurface Surveys, 1990).

Locally as mapped by Hernandez and Tan (2007), the subject site is shown to be underlain by late Pleistocene age older alluvium. These deposits are generally described as being comprised of a fine- to medium-grained sand and fine to medium gravel of inactive fans.

CBC Ground Motion Analysis

Included for this study was an assessment of the seismic ground motion parameters of the subject site with respect to the most recently adopted 2022 California Building Code (CBC) and ASCE/SEI Standard 7-22 (ASCE, 2022) as partially summarized and tabulated below. Geographically, the proposed construction area is centrally located at Latitude 34.610365 and Longitude -117.196553.

<u>Site Classification (CBC 1613.3.2)</u> – Based on the presence of mapped Quaternary age alluvial deposits underlying the site and the absence of site-specific shear-wave data, the design Site Class is *estimated* to be **"D."** This Class is defined as having the upper 100 feet (30 meters) of the subsurface being underlain by "Stiff Soil" with average shear-wave velocities of 600 to 1,200 feet/second (180 to 360 meters/second). In accordance with the CBC, the proposed warehouse is considered a Risk Category II structure.

TABLE 1: SUMMARY OF SEISMIC DESIGN PARAMETERS										
Factor or Coefficient	Value									
Ss	1.16g									
S ₁	0.39g									
S _{DS}	1.0g									
S _{D1}	0.67									
S _{MS}	1.5g									
S _{M1}	1.0									
Τι	12 Seconds									
PGA _M	0.55g									
V _{S30}	260									
Site Class	D									

Groundwater

The study area lies within the Upper Mojave River Groundwater Basin of southern California. The Mojave River Basin is part of the Mojave Desert region and is bordered by the San Bernardino and San Gabriel Mountains to the south and extends to Afton Canyon to the northeast, with Lucerne Valley and Antelope Valleys bordering the east and west, respectively. The Mojave River, which is located to the west, is the principal source of water recharge to the basin, which originates from the junctions of Deep Creek and West Fork Mojave River at the northern foot of the San Bernardino Mountains. Other sources of recharge include other lesser river tributaries from the San Bernardino and San Gabriel Mountains, the adjacent highlands to the north and east, as well as deep percolation from rainwater and other artificial means.

The water-bearing deposits are principally unconsolidated and partially consolidated continental sedimentary deposits that form two aquifers (Stamos and Predmore, 1995), the upper one being shallow alluvium (200± feet thick, within 1± mile of the Mojave River), with the regional aquifer underlying most of the basin at depth. The regional aquifer is comprised of unconsolidated older alluvium and fan deposits of Pleistocene to Tertiary age, and partly consolidated to consolidated sediments of Tertiary age. These deposits are as much as 1,000 feet thick in some places and their permeability generally decreases with depth.

Based on groundwater data provided by the California Department of Water Resources (2023), the closest measured well is approximately 1,300± feet to the west (State Well No. 06N03W16C001S), which had a water level of 39 feet in 1957 (only measurement). Other wells in the nearby vicinity show groundwater depth around 87 feet in depth (State Well No. 06N03W16D001S) located approximately 2,400± feet to the west, and 52 feet in depth (State Well No. 06N03W09N001S) located approximately 2,400± feet to the northwest.

Faulting

There are at least thirty-five major "potentially active/active" (late Quaternary) faults that are within a 100-kilometer (62 mile) radius of the site as shown on Figure 1 below (site shown as small dot in middle).



FIGURE 1: Regional Fault Map showing 100 km radius (from CGS 2002 California Fault Model)

Of these, there are no active faults known to traverse the site based on published literature. In addition, the subject site is not located within a State of California "Alquist-Priolo Earthquake Fault Zone" for surface fault rupture hazards (CGS, 2018).

The nearest mapped "active" fault zoned by the State of California is for the Helendale-South Lockhart Fault, located approximately $2\frac{1}{2}\pm$ -miles to the northeast. The Helendale-South Lockhart Fault is a right-lateral, strike-slip fault, being approximately 97 kilometers in length, with an associated slip-rate of 0.6 ±0.4 mm/year (C.D.M.G., 1996 and Cao, et al., 2003).

CONCLUSIONS AND RECOMMENDATIONS

The existing surface soils are medium dense to a depth of about 3 feet. Below 3 feet, the native soils are generally dense and are considered adequate for support of the new facilities.

The site is not within an Alquist Priolo Earthquake Fault Zone. The soils are medium dense to dense, and groundwater is deep below this site. The liquefaction potential consequently is very low. The potential for dynamically induced settlement of the granular soils is also very low. In addition, the soils have a very low potential for expansion due to changes in moisture content.

The potential for encountering groundwater within the anticipated relatively shallow excavations is minimal. There is a potential for minor amounts of water to enter open excavations because of direct rainfall and runoff.

Earthwork

At the time of MJG's investigation, the site was covered with sparce desert vegetation. Any debris, vegetation, and other deleterious materials should be stripped and removed from the site prior to grading work. Organic materials should be disposed of off-site in accordance with the owner's instructions. Roots should be removed to a depth of 6 inches below foundation and pavement subgrade elevations.

Areas to receive fill should be scarified to a depth of 12 inches, brought to within 2 percentage points above or below optimum moisture content, and compacted to a minimum of 95% relative compaction based on the ASTM D1557 laboratory test method. All references to optimum moisture content and relative compaction in this report are based on this test method.

Compacted Fill Placement

Fill should be placed in 8-inch-thick loose lifts, moisture conditioned to within 2 percentage points above or below optimum moisture content and compacted to a minimum of 95% relative compaction.

Imported Soils

Imported soils, if needed, should consist of predominantly granular material with an expansion index less than 20 when tested in accordance with ASTM D4829, and should have a minimum R-value of 40. Imported material should be inspected and approved by an MJG's representative prior to being brought to the site.

Shallow Foundation and Building Slab-On-Grade Support

The existing soils below and within five (5) feet of the proposed warehouse building should be over-excavated to a depth of at least three feet below the existing ground surface or 12 inches below the proposed footing base grade, whichever depth is greater. The bottom of the overexcavation should be scarified to a depth of at least 6 inches, moistened to within 2 percent of the optimum moisture content, and compacted to a relative compaction of at least 95 percent (ASTM D 1557).

Fill should be placed in 8-inch-thick loose lifts, moisture conditioned to within 2 percentage points above or below optimum moisture content and compacted to a minimum of 95% relative compaction.

The planned structures can be supported on shallow spread footings with bottom levels in the compacted fill at a minimum depth of 18 inches below the lowest adjacent finished grade.

A minimum width of 18 inches is recommended for continuous footings. Isolated footings should be at least 24 inches wide. Footings can be designed for an allowable bearing pressure of 2500 pounds per square foot (psf) for dead plus long-term live loads. This value can be increased by ¹/₃ when considering the total of all loads, including wind or seismic forces.

Total post-construction settlement is estimated to be approximately $\frac{3}{4}$ inch. Post-construction differential settlements are anticipated to be $\frac{1}{2}$ inch or less between isolated footings, and between the middle and end of a continuous footing.

Continuous (strip) foundations should be reinforced with a minimum of #5 deformed reinforcing bars at the top and bottom of the footings.

Spread footing reinforcement should be designed by the structural engineer for punching shear and bending. As a minimum, the spread footings should be reinforced with a #5 deformed reinforcing bars, spaced 18 inches on center each way and placed 3 inches above the bottom of the spread footing.

All grade beam reinforcement should be designed and specified by the building's designer/structural engineer.

Foundations should be reinforced as necessary to reduce the potential for distress caused by differential foundation movement. The use of joints at openings or other discontinuities in masonry walls is recommended.

Footing excavations should be observed by an MJG's representative to check bearing materials and cleaning.

Lateral Loading

Resistance to lateral loads will be provided by passive earth pressure against the faces of footings and other structural elements below grade, and by friction along the bases of footings and slabs. Passive earth pressure can be taken as 350 pounds per square foot (psf) per foot of depth. Base friction can be taken as 0.35 times the actual dead load. Base friction and passive earth pressure can be combined without reduction. Retaining structures free to rotate at the top should be designed for an active equivalent fluid pressure of 35 psf per foot of height, plus any additional building or equipment surcharge. MJG should be notified if retaining walls greater than 10 feet in height, restrained walls, or tieback walls are planned so that geotechnical recommendations specific to wall conditions can be developed.

Building Floor Slabs

During grading operations, the building pad soils should be compacted to a relative compaction of at least 95 percent (ASTM D 1557). Prior to placing the slab-on-grade concrete, the final pad surfaces should be proof-rolled to provide a smooth, dense surface upon which to place the concrete.

A 15-mil vapor retarder membrane, conforming to ASTM E 1745 and installed per ASTM E 1643, should be placed beneath concrete slabs-on-grade covered with moisture sensitive or impervious floor coverings, or where the slab will support equipment or materials sensitive to moisture. When conditions warrant the use of a vapor retarder, the slab designer should refer to

ACI 302 and/or ACI 360 for procedures and cautions regarding the use and placement of a vapor retarder.

Reinforcing for slabs-on-grade should be designed by the project structural engineer based on anticipated storage and forklift loads. A modulus of subgrade reaction of 150 pounds per cubic inch (pci) can be used. Reinforcing should extend down into the footings. Concrete construction (i.e. jointing, etc.) should be in conformance with the American Concrete Institute Manual of Concrete Practice Design and Construction Standards.

Minimum reinforcing for 4-inch-thick slabs-on-grade should consist of 6" x 6" W1.4 /1.4 welded wire fabric supported mid height in the slab by concrete blocks or dobies. Positioning the wire fabric by lifting after concrete placement should not be allowed. Minimum reinforcing for 6-inch-thick slabs-on-grade should consist of at least #4 deformed reinforcing bars at 12 inches on center each way placed at mid-height in the slab.

Where the project's structural engineer's reinforcement recommendations exceed MJG's above minimum slab reinforcement recommendations, the structural engineer's recommendations should be followed.

Saw-cut control joints should be placed in the slab to help control the location and extent of cracking. For additional recommendations refer to the ACI Design Manual. Joints or cracks should be sealed with a waterproof, non-extruding compressible compound specifically recommended for heavy duty concrete pavement and wet environments.

Where floor slabs are tied to perimeter walls or turn-down slabs to meet structural or other construction objectives, our experience indicates differential movement between the walls and slabs will likely be observed in adjacent slab expansion joints or floor slab cracks beyond the length of the structural dowels. The structural engineer should account for potential differential settlement through use of sufficient control joints, appropriate reinforcing, or other means.

Surface Drainage

It is important that water be kept a minimum of 5 feet from structures and slabs. No ponding adjacent to buildings and structures should be allowed. Final surfaces should have a positive 2 percent minimum slope away from structures.

Retaining walls should be designed to resist hydrostatic pressures or be provided with a backdrain, weep holes or other drainage facilities. If a basement or underground structure is constructed, a subsurface drainage system is recommended.

Concrete and Flexible Asphalt Concrete Pavement Subgrade Preparation

Soils should be scarified to a depth of at least 12 inches, moistened to within 2 percent of the optimum moisture content and compacted to a relative compaction of at least 95 percent (ASTM D1557). Any additional fill required to prepare the finish subgrade should be placed in maximum 8-inch-thick lifts, each lift moistened to within two (2) percent of the optimum moisture content and compacted to a relative compaction of at least 95 percent.

Flexible Pavement Structural Sections

New flexible pavement structural sections were determined following California Department of Transportation (Caltrans) procedures.

ONSITE FLEXIBLE PAVEMENT

Onsite flexible pavement for automobiles and light trucks are planned for the north and south sides of the project site. MJG's review of the Conceptual Site Plan indicates that most of the heavy truck driveways, trailer parking areas, and loading docks will be located on the east and west sides of the warehouse and paved with rigid portland cement concrete pavement. The automobile and truck trailer parking areas will be connected by onsite access driveways.

Six test borings were drilled around the perimeter of the proposed warehouse. Sieve analyses (ASTM D422, D1140 & D2487) and sand equivalent tests (ASTM D 2844) were performed from soil samples collected in each of these borings. The soil samples containing the largest percentage of fines (soil fraction passing the #200 sieve) and the lowest sand equivalent value were selected and tested for R-value (ASTM D 2844).

The most critical soil samples were collected in Boring Nos. 10 and 12 located on the east and west sides of the warehouse, respectively. R-value tests were performed from the soil samples collected in these two borings. The sieve analysis, sand equivalent, and R-value test data are summarized in Table 2 below.

TABLE 2: ONSITE SIEVE AND R-VALUE TEST RESULTS											
Boring No.% Passing the 200 Sieve (ASTM D422, D1140, & D2487)Sand Equivalent ASTM D 2844R-value ASTM D284											
8	10.1	71									
9	12.4	36									
10	13.9	24	25								
11	18.4	24									
12	17.4	17	17								
13	14.9	37									

Based on the above soil test data, the most critical R-value of 17 was used to calculate the recommended onsite flexible pavement sections for the project. In addition, the Traffic Indexes for the flexible pavement areas was selected as follows:

- Automobiles and light truck traffic: TI = 5
- Heavy truck traffic: TI = 8

Recommended onsite flexible pavement structural sections are listed in Table 3 below.

TABLE 3: ONSITE FLEXIBLE PAVEMENT STRUCTURAL SECTIONS									
Pavement Area Traffic Index Asphalt Concrete (inches) Base Course									
Autos & Light Truck Traffic	5	3	8						
Heavy Truck Traffic	6	12							

OFF-SITE FLEXIBLE PAVEMENT FOR CARDOVA AND DACHSHUND AVENUE

Off-site flexible pavement is proposed for Cardova Road and Dachshund Avenue adjacent the subject warehouse site. Additionally, the paving of Cardova and Dachshund Avenue will be extended from the southwest corner of the warehouse site westward to Dale Evans Parkway and southward to Johnson Road, respectively.

Two test borings were excavated along the alignment of Cardova Road and two along Dachshund Avenue (4 total). Samples from the four test borings were collected and tested for sieve analysis (ASTM D422, D1140 & D2487). The samples containing the largest percentage of fines from each street (soil fraction passing the #200 sieve) were selected and tested for R-value (ASTM D 2844).

The most critical soil samples were collected in Boring Nos. 14 and 15 located on Cardova Road and Dachshund Avenue, respectively. R-value tests were performed from the soil samples collected in these two borings. The sieve analysis and R-value test data are summarized in Table 4 below.

TABLE 4: OFF-SITE ROADWAY SIEVE AND R-VALUE RESULTS													
Boring No.	% Passing the 200 SieveR-valueBoring No.Roadway(ASTM D422, D1140, & D2487)ASTM D2844												
14	Dachshund Avenue	23.4	58										
15	Cardova Road	27.4	52										
16	Cardova Road	15.4											
17	Dachshund Avenue	20.1											

Based on the above soil test data, the most critical R-values of 52 and 58 were used to calculate the recommended off-site flexible pavement sections for Cardova and Dachshund Avenue, respectfully. The Traffic Index used to calculate the roadway pavement sections was:

• Automobiles and Heavy truck traffic: TI = 9

Recommended off-stie flexible pavement structural sections for Cardova and Dachshund Avenue are presented in Table 5 below.

TABLE 5: ONSITE FLEXIBLE PAVEMENT STRUCTURAL SECTIONS									
Roadway Traffic Index Asphalt Concrete Base Course (inches) (inches)									
Cardova Road	9	5	6						
Dachshund Avenue	9	5.5	4						

Alternative pavement sections can also be considered. Merrell Johnson should review the design pavement sections if traffic loads will be different from those currently anticipated.

PORTLAND CEMENT CONCRETE PAVEMENTS AND FLATWORK

The subgrade surface beneath rigid (portland cement concrete) pavements should be proofrolled with a smooth-wheel roller to form a dense, uniform surface. Any pumping or yielding areas should be excavated and replaced with compacted fill.

Rigid pavements to support <u>automobile and light truck traffic</u> should be a minimum of 6 inches thick and reinforced with a minimum of #4 deformed reinforcing bars spaced 12 inches on center each way. Joints should be provided at intervals of no more than 12 feet. Smooth dowels should be provided across pavement joints.

Rigid pavement to support <u>heavy truck traffic</u> should be a minimum of 8 inches thick and reinforced with #4 deformed reinforcing bars spaced 12 inches of center each way. Joints should be provided at intervals of no more than 12 feet. Smooth dowels should be provided across pavement joints.

Pedestrian walkways and other lightly loaded concrete flatwork areas should be proof rolled as described above. The flatwork in these areas should have a minimum thickness of 4 inches and be provided with doweled joints at no more than 12-foot intervals. Minimum reinforcement should consist of 6 x 6 W1.4/1.4 welded wire fabric supported mid height in the slab by concrete blocks or dobies. Positioning the wire fabric by lifting after concrete placement should not be allowed.

UTILITY EXCAVATIONS

Excavations for this project will require sloping sidewalls or shoring. Excavations should be made in accordance with California Administrative Code, Title 8, Industrial Relations, Chapter 4, Division of Industrial Safety, Subchapter 4, Construction Safety Orders, Article 6. Temporary excavations should be shored or sloped in accordance with Cal OSHA requirements. On-site soils can be considered Type C for purposes of excavation design.

In general, temporary excavations in on-site soils should be sloped no steeper than 1.5 horizontal to 1 vertical for excavations up to 20 feet in depth. Compound excavations with vertical sides in lower portions should be properly shielded to a minimum height of 18 inches above the top of the vertical side, with the upper portion having a maximum slope of 1.5 horizontal to 1 vertical. A Registered Professional Engineer should design slopes or benching for excavations greater than 20 feet in depth.

Temporary excavation slopes should be inspected twice daily by the contractor's competent person before personnel are allowed to enter the excavation. If sloughing, raveling or other evidence for slope instability is noted, corrective measures should be implemented.

Temporary shoring will be required for those excavations where temporary cut slopes as described above are not feasible. Cantilever shoring, and shoring with 1 level of bracing, can be designed to resist an equivalent fluid pressure of 30 psf per foot of depth. For shoring with multiple levels of bracing, a uniform lateral pressure equal to 25H in psf, where H is the height of shoring in feet, should be used. The recommended soil pressure applies to level soil conditions behind the shoring. Where a combination of sloped embankment and shoring is used, the soil pressure will be greater and should be evaluated for actual conditions.

In addition to the above recommended lateral earth pressures, a minimum uniform lateral pressure of 125 psf should be incorporated in the design of the upper 10 feet of shoring when normal traffic is permitted within 10 feet of the shoring. The design of temporary shoring should also include the surcharge loads from delivery and construction equipment, as appropriate.

CORROSIVITY

Laboratory test results indicate that resistivity of the soils sampled exhibit resistivities ranging from 260 to 1,500 ohms-cm, which indicates the soils have a corrosion potential with respect to reinforced concrete and ferrous metals. For this reason, Type II modified, or Type V cement is recommended for use in concrete in contact with the ground. Foundations should be designed with continuous reinforcing steel top and bottom. Reinforcing steel should maintain minimum clearances specified by applicable codes and good construction practice. Appropriate corrosion protection, including consultation with a qualified corrosion engineer, should be implemented anywhere ferrous metal is in contact with the soils.

LIMITATIONS

The recommendations in this report are based on results of the field exploration and laboratory test programs, combined with interpolation and extrapolation of subsurface conditions between and beyond boring locations. The nature and extent of variations in these conditions may not become evident until construction. If variations are encountered during construction, MJ should be notified so these variations can be reviewed and the recommendations in this report modified if necessary. If changes in the nature, design or location of the structures are planned, these changes should be reviewed by MJ so that modifications to the recommendations in this report can be made if needed.

Our professional services have been performed using the degree of care and skill ordinarily exercised under similar circumstances by reputable engineering consultants practicing in this or similar localities. No other warranty, express or implied, is made as to the professional advice or data included in this report. This report has not been prepared for use by other parties and may not contain sufficient information for purposes of other parties or other uses.

APPENDIX A

Figure 1 – Site Vicinity Map Figure 2 – Plot Plan / Satellite Site Image Figure 3 – Architectural Site Plan Figure 4 – Conceptual Grading Plan ande

Black Mountain Quarry Plant

Bell Mountain

DESERT KNOLLS

/icto







This conceptual design is based upon a preliminary review of entitlement requirements and on unverified and possibly incomplete site and/or building information, and is intended merely to assist in exploring how the project might be developed.

~____L_____/

Boundary Source: PDF ALTA SURVEY

------Stormwater Management Design:

SCHEME: 03

DEVELOPMENT STANDARDS

Zoning		
Jurisdiction		Apple Valley, CA
Zoning Designation		I-SP (Specific Plan)
Max Coverage		45% 4
Max Height		100 FT
Building Setbacks		1
Landscape Setbacks		2
Parking Standards		
	Min Stall Size	9X19
	Drive Aisle	24 FT
Required Parking		
	Office	1/250 SF 5
	Manufacturing	1/500 SF 3
	Non-Specified	3/1000 SF 6
	Warehouse	1/500 SF 2
	≤10000 SF	1/500 SF
	10000># SF	1/1000 SE
PROJECT DATA	10000_// 01	1/ 1000 01
Site Summary		
Gross Site Area	3,927,102 SF	90.15 AC
Total Building Area(s)	Gross Floor Area	1,373,150 SF
0 ()	Footprint	1,346,270 SF
Coverage	Gross	34%
FAR	Gross	0.35
Building 1		
Building Area(s)	Footprint	1,346,270 SF
	Mezzanine	26,880 SF
	Gross Floor Area	1,373,150 SF
Cars Required	@4% Office	1,383 Stalls
Cars Provided	@1.05/1,000 SF	1,440 Stalls
	Req. Accessible	29 Stalls
Drive-in Doors		4
Docks	@1.63/10,000 SF	224
Trailers		619 Stalls
Notes		
1. From major or secondary streets, th	ne setback is 50 FT. From local indu	strial streets, the setback is

2. 1 space per 500 SF of GFA for the first 10,000 SF and beyond that, 1 space per 1,000 SF of GFA; for office area that exceeds 25%, provide 1 space per 200 SF in excess of 25%

3. 1 space per 500 SF of GFA or 1 space per 2 employees on the largest shift, whichever is greater; for office area that exceeds 25%, provide 1 space per 200 SF in excess of 25%4. To be determined by city.

5. Minimum required number of parking spaces: 4

6. 3 spaces per 1000 SF of GFA or 1 space per 2 employees on the largest shift, whichever is greater; for office area that exceeds 25%, provide 1 space per 200 SF in excess of 25%

Conceptual Site Plan Redwood West Cordova Apple Valley Cardova Rd, Apple Valley, CA 92307

WARE MALCOMB

APPENDIX B

Exploratory Logs

Soil Classification Key

Unified Soil Classification System (USCS) and Particle Size Limits

Project Number: Project Title: Project Location: Client: 3813.006.500 Industrial Building Apple Valley, CA Redwood West

 Report Date:
 12

 Sheet:
 12

 Appendix:
 B

 Permit No:
 Client Project No:

 Other:
 DSA File No:

 DSA Application No:
 DSA LEA No:

12/01/23 1 of 1

1 01

Client:		Redwood	West		DSA LEA No:							
					Unified S	oil Classification System	(USCS)					
	Gravel	C Gr	lean avels	GW Well-graded gravels, gravel-sand mixtures, little or no fines								
	Grave	elly ^{Little}	e Or No	GP	GP Poorly-graded gravels, gravel-sand mixtures, little or no fines							
Coarse	More Than Retained o	n 50% Grav	vels w/ ines	GM		Silty gravels, gravel-sand-silt mixtures						
Grained Soils	4 Slev	App Ar	reciable mount	GC		Clayey gravels, gravel-sand-clay mixtures						
More Than 50% Is Larger Than No. 200 Sieve	Sand a	Clea	an Sand	SW		Well-graded sands, grave	elly sands, little or no fines					
	Sand Soils	ly F	Fines			Poorly-graded sands, gravelly sands, little or no fines						
	More Than Passing N	^{1 50%} Sar No. 4 F	nds w/ ines	SM	SM Silty-sands, sand-silt mixtures							
	31676	App Ar	reciable mount	SC Clayey sands, sand-clay mixtures								
	Silts and			ML		Inorganic silts and very fi slight plasticity	ne sands, rock flour, silty or clayey	/ fine sands or clay	ey silts with			
	Clays Liquid Limit	Clays Liquid Limit Less		CL		Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays						
Fine Grained	Than 5	50		OL	OL Organic silts and organic silty clays of low placticity							
SOIIS More Than 50% Is Smaller Than	Silts a	Ind		MH		Inorganic silts, micaceou	s or diatomaceous fine sand or silt	y soils				
No. 200 Sieve	Clay: Liquid Li	Clays Liquid Limit CH Inorganic clays of high				Inorganic clays of high pla	asticity, fat clays					
	Greater Th	nan 50		ОН		Organic clays of medium to high plasticity, organic silts						
	Hig	ghly Organic So	oils	PT		Peat, humus, swamp soil	s with high organic contents					
						Particle Size Limits						
Divison		Silt or Clay			Sa	nd	Gravel	Cobbles	Boulders			
	Fine Medium Coarse Fine Coarse											

Grain (mm) 0.075 0.420 2.00 4.76 19.1 76.2 305

No. 10

Soils possessing characteristics of two classifications are designated by group symbol combination. Soils may be classified initially using the visual manual procedure prior to laboratory test.

No. 40

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No. 200

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3"

12"

U.S. Sieve

3/4"

No. 4

Exploratory Log ASTM D5434, D1452, D1586, D1587, D2488 (USCS), D3550										rt Date: :: ndix: it No:	12/01/23 1 of B	2	
Project Number:3813.006.500Client Project No: USA Ticket No: DSA File No: DSA File No: DSA Application No: DSA LEA No:Project Location:Apple Valley, CA Redwood WestDSA LEA No:													
Loc	ation No	:	B1			St	art Date/Time:	10/25/23 0	730	End Date/Time	e: 1()/25/23 0825	
Con Ope Equ Driv Driv	Conducted By:J. AlbornozOperator:A. LaraEquipment Type:CME-75-HSADrive Weight (lb):140Drive Drop (in):30				oz ISA	Ex Di Ac Fic Sh	Excavation Type:Auger HoleElevation:2Dimensions:8" x 50'Groundwater:1Advance Assist:NoneRecent Weather:0Field Tests:D3550Sampler Insertion:[Shoring Type:NonePreservation:[28 N er: C ion: D D	368 ot Encountered ear riven 4220	
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comm	nents		Lab Tests ⁽²⁾	
0	20, 21, 26 30, 32, 50 32, 50 (3") 50 (4") 50 (5")		4.1 4.6 3.2 2.8	95.4 96.6 99.3 104.8	SPSM		Light Brown, Dry, I Bulk Sample at 0' t Tube Sample at 1' Tube Sample at 3'- Tube Sample at 5' Light Brown, Dry, V Tube Sample at 10	ght Brown, Dry, Dense, Silty Sand ulk Sample at 0' to 5' - JDA10252301 ube Sample at 1' - JDA10252302 ube Sample at 3'- JDA10252303 ube Sample at 5' - JDA10252304 ight Brown, Dry, Very Dense, Poorly Graded Sand with Silt					
20 -	50 (4")						SPT at 20', No Red	covery					
25 -	50 (3")						SPT at 25', No rec Difficulty Drilling	overy					
Con	nments: ountered c	"N" Valu Iurina dri	e Based o Ilina oper	on 2.5" dia ations. P	ameter n artial cav	nodified (rina of ho	California Tube Sam le observed.	pler (ASTM D3550)) or SPT (A	ASTM D1586) as r	noted on log. Se	ome boulder/rock	
(1)	=Bulk =Drive	n	⁽²⁾ DS EI	=DirectShe =Expansion	ar Index	SA CR	=Sieve Analysis =Corrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density	

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Exploratory Log ASTM D5434, D1452, D1586, D1587, D2488 (USCS), D3550 Project Number: 3813.006.500										Report Date:12/01/23Sheet:2Appendix:BPermit No:Client Project No:USA Ticket No:			
Project Title:Industrial BuildingDSA File No:Project Location:Apple Valley, CADSA Application No:Client:Redwood WestDSA LEA No:													
Loc	Location No: B1 (Cont.) Start Date/Time: 10/25/23 0730 End Date/Time: 10									0/25/23 0825			
Cor Ope Equ Driv Driv	nducted erator: upment T ve Weigh ve Drop (i	Ву: Гуре: t (Ib): n):	J. A A. 1 CM 140 30	Alborn Lara IE-75 H 0	oz HSA	E) Di A(Fi Sł	ccavation Type: mensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 50' None D3550 None	Elevation: Groundwater: Recent Weath Sampler Insert Preservation:	er: (ion: [2868 Not Encountered Clear Driven D4220		
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comm	ents		Lab Tests (2)	
30 - 35 - 40 - 45 - 50 - 55 -	50 (2') 50 (3") 50 (2") 50 (2")				313101		SPT at 40' SPT at 40' Very Difficult Drill SPT at 50' *Drilling Terminal	countered ling ted at Approximately	50'*				
Cor	mments: ountered o	"N" Valu durina dr	ue Based (illina oper	on 2.5" d rations. F	iameter n Partial cav	nodified (/ina of ho	California Tube San le observed.	npler (ASTM D3550)	or SPT (A	STM D1586) as r	noted on log.	Some boulder/rock	
(1)	=Bulk =Drive	'n	⁽²⁾ DS EI	=DirectSh =Expansior	ear n Index	SA	 =Sieve Analysis =Corrosion 	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN TD	=Consolidation =Tube Density	
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Exploratory Log ASTM D5434, D1452, D1586, D1587, D2488 (USCS), D3550										Report Date: 12/01/23 Sheet: 1 of 1 Appendix: B Permit No:			
Project Number:3813.006.500ClieProject Title:Industrial BuildingDSAProject Location:Apple Valley, CADSAClient:Redwood WestDSA													
Loc	Location No: B2 Start Date/Time: 10/25/23 0920 End Date/Time:									: 10	0/25/2023 095(
Con Ope Equ Driv Driv	iducted I erator: ipment 1 e Weight e Drop (ii	By: Type: t (Ib): n):	J. A A. I CM 140 30	Alborno Lara IE-75 F)	oz ISA	Ex Dir Ac Fie Sh	cavation Type: mensions: Ivance Assist: eld Tests: oring Type:	Auger Hole 8" x 25' None D3550 None		Elevation: Groundwater: Recent Weathe Sampler Inserti Preservation:	20 N er: C ion: D D	369 ot Encountered lear riven 4220	
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comme	ents		Lab Tests ⁽²⁾	
0 - - - - - - - - - - - - - - - - - - -	10, 10 11 10, 12, 18 27, 50 (3") 50 (3") 50 (3") 50 (3")		3.4 2.5 3.9	94.2 107.2 96.7	SPSM		Light Brown, Dry, Bulk Sample at 0' Tube Sample at 3' Tube Sample at 5' Very Dense Bulk Sample at 5' Light Brown, Dry, Tube Sample at 10 SPT at 15' Bedrock Encounte SPT at 20' SPT at 20'	Description / Comments ight Brown, Dry, Medium Dense, Silty Sand 3ulk Sample at 0' to 5' - JDA10252306 Fube Sample at 1' - JDA10252307 Fube Sample at 3' - JDA10252308 Fube Sample at 5' - JDA10252309 /ery Dense 3ulk Sample at 5' to 10' - JDA10252310 .ight Brown, Dry, Very Dense, Poorly Graded Sand with Silt Fube Sample at 10' - No Recovery SPT at 15' 3edrock Encountered SPT at 20' SPT at 25' 'Drilling Terminated at Approximately 25'*					
Con	nments:	"N" Valu lurina dri	e Based o Ilina oper	on 2.5" di ations. P	ameter n artial cav	nodified C	alifornia Tube San observed.	npler (ASTM D3550)	or SPT (A	STM D1586) as n	oted on log. S	eme boulder/rock	
(1)	=Bulk =Drive	n	⁽²⁾ DS EI	=DirectShe =Expansion	ar Index	SA CR	=Sieve Analysis =Corrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density	
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		ASTM	E D5434,	xplc D1452, C	orat 1586, D	Ory 01587, D2	Log 488 (USCS), D355()	Report D Sheet: Appendi Permit N	Pate: x: o:	12/01/23 1 of B	1	
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Loc	ation No	:	B3			St	art Date/Time:	10/25/23 1	010 e	End Date/Tim	e: 1	0/25/23 1040	
Cor Ope Equ Driv Driv	nducted I erator: lipment 1 ve Weight ve Drop (i	By: 「ype: t (Ib): n):	J. A A. 1 CM 140 30	∖lbornc Lara E-75 ⊦)	oz ISA	E) Di Ao Fi	cavation Type: mensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 25' None D3550 None	E C F S F	Elevation: Groundwater: Recent Weath Sampler Inser Preservation:	: N her: C tion: D	863 ot Encountered lear riven 4220	
Depth (ft)	Depth (ft) 											Lab Tests ⁽²⁾	
	35, 50 (5") 33, 30, 34 19, 26, 39 33, 50 (4") 50 (4") 50 (4") 50 (4")		4.37.76.52.9	98.0 84.3 85.2 97.5			Light Brown, Dry, Bulk Sample at 0' Tube Sample at 3' Whitish brown Tube Sample at 5' Tube Sample at 5' Tube Sample at 10 Light Brown, Dry, SPT at 15' SPT at 20' SPT at 20'	Very Dense, Silty Sa to 5' - JDA10252311 - JDA10252312 - JDA10252313 - JDA10252314 0' - JDA10252315 Very Dense, Poorly (ecovery ed at Approximately	ind Graded Sand 25 ¹ *	with Silt		MD, CR, EI TD TD TD	
Con	Comments: "N" Value Based on 2.5" diameter modified California Tube Sampler (ASTM D3550) or SPT (ASTM D1586) as noted on log. Some boulder/rock encountered during drilling operations. Partial caving of hole observed.												
(1)	(1) =Bulk (2) DS = Direct Shear SA = Sieve Analysis MD = Max Density AL = Atterberg Limits CN = Consolidation = Driven EI = Expansion Index CR = Corrosion RV = R-Value SE = Sand Equivalent TD = Tube Density												
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Merrell Engineering Company, Inc. | 22221 US Highway 18, Apple Valley, Ca. 92308 t)760.256.2068 f)760.256.0418 w)www.merrelljohnson.com

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Depth (ft)	Depth (ft) N. Value N. Value N. Value Noisture (%) Moisture (%) Mo											Lab Tests ⁽²⁾	
0	50 (6") 50 (4") 50 (2") 50 (3") 50 (4") 50 (4")		2.6	102.0			Light Brown, Dry, Bulk Sample at 0' Tube Sample at 3' Tube Sample at 5' Grayish Brown, P Bedrock Encounte Tube Sample at 10 SPT at 15' SPT at 20' SPT at 20'	Poorly Graded Sand to 5' - JDA10252315 - JDA10252316 (On - No Recovery oorly Graded Sand red 0' - No Recovery 0' - No Recovery	with Silt e Tube Rec 25'*	covered)		MD, DS TD	
Cor	Comments: "N" Value Based on 2.5" diameter modified California Tube Sampler (ASTM D3550) or SPT (ASTM D1586) as noted on log. Some boulder/rock encountered during drilling operations. Partial caving of hole observed.												
(1)	(1) =Bulk (2) DS =Direct Shear SA =Sieve Analysis MD =Max Density AL =Atterberg Limits CN =Consolidation =Driven EI =Expansion Index CR =Corrosion RV =R-Value SE =Sand Equivalent TD =Tube Density												
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Loc	ation No	:	B5			St	art Date/Time:	10/25/23 1	155	End Date/Time:	1(0/25/23 1220
Cor Ope Equ Driv Driv	nducted I erator: lipment 1 ve Weight ve Drop (ii	By: 「ype: t (Ib): n):	J. A A. 1 CM 140 30	Alborno Lara IE-75 F 0	oz ISA	Ex Di Ad Fid Sh	acavation Type: mensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 25' None D3550 None		Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	20 N C D	863 ot Encountered lear riven 4220
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comn	nents		Lab Tests (2)
	50 (6") 50 (4") 50 (6") 50 (6") 50 (3") 50 (3")		3.7 2.8 4.2	104.6 101.6 96.8			Light Brown, Dry, Bulk Sample at 0' Tube Sample at 1' Tube Sample at 5' Light Brown, Dry, Bedrock Encounte Tube Sample at 10 SPT at 15' Difficulty Drilling SPT at 20' - No Re SPT at 25' *Drilling Terminat	Silty Sand to 5' - JDA10252317 ' - JDA102523219 (O Poorly Graded Sand ared 0' - JDA10252320 (O o' - JDA10252320 (O ecovery	ne Tube F with Silt ne Tube F 25'*	Recovered) Recovered)		SA TD TD TD
Cor	Comments: "N" Value Based on 2.5" diameter modified California Tube Sampler (ASTM D3550) or SPT (ASTM D1586) as noted on log. Some boulder/rock											
(1)	encountered during drilling operations. Partial caving of hole observed.											

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		ASTM	E 2 1 D5434, 1	xpic D1452, C)rat)1586, D	OTY 1587, D2	Log 488 (USCS), D3550	0	Repor Sheet: Apper Permit	t Date: 12 ndix: B : No:	2/01/23 1 of	1	
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Loca	ation No	10)/25/23 1300										
Con Ope Equi Driv Driv	ducted rator: ipment ⁻ e Weigh e Drop (By: Type: t (Ib): in):	J. A A. I CM 140 30	\lbornc _ara Æ-75 ⊦)	∋z ⊣SA	E) Di Ao Fi	acavation Type: mensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 10' None D3550 None		Elevation: Groundwater: Recent Weather: Sampler Insertion Preservation:	28 No Cl Di D ²	362 ot Encountered ear iven 1220	
Description / Comments										ents		Lab Tests ⁽²⁾	
							Bulk Sample at 5'	to 10' - JDA1025232'	1 10'*			SA	
Con enco	Comments: "N" Value Based on 2.5" diameter modified California Tube Sampler (ASTM D3550) or SPT (ASTM D1586) as noted on log. Some boulder/rock encountered during drilling operations. Partial caving of hole observed.												
(1)	(1) =Bulk (2) DS =Direct Shear SA =Sieve Analysis MD =Max Density AL =Atterberg Limits CN =Consolidation =Driven EI =Expansion Index CR =Corrosion RV =R-Value SE =Sand Equivalent TD =Tube Density												
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Loca	Location No: B7 (Perc.) Start Date/Time: 10/25/23 1315 End Date/Time:												
Con Ope Equ Driv Driv	nducted erator: ipment ⁻ re Weigh re Drop (By: Type: t (lb): in):	J. A A. I CM 140 30	Alborno Lara IE-75 F)	oz HSA	E) Di A(Fi Sł	ccavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 10' None D3550 None		Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	28 N C D D	363 ot Encountered ear riven 4220	
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	n / Comm	ents		Lab Tests ⁽²⁾				
							Light Brown, Dry, Rock Encountered Bulk Sample 5' to	Poorly Graded Sand 1 10' - JDA10252322 red at Approximately	10'*			SA	
Con enco	Comments: "N" Value Based on 2.5" diameter modified California Tube Sampler (ASTM D3550) or SPT (ASTM D1586) as noted on log. Some boulder/rock encountered during drilling operations. Partial caving of hole observed.												
(1)	(1) =Bulk (2) DS = Direct Shear SA = Sieve Analysis MD = Max Density AL = Atterberg Limits CN = Consolidation = Driven EI = Expansion Index CR = Corrosion RV = R-Value SE = Sand Equivalent TD = Tube Density												
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		ASTN	E 1 D5434, 1	xplc D1452, [)rat 01586, D	OTY 1587, D2	Log 488 (USCS), D3550)	Repor Sheet: Apper Permit	t Date: 12/ : 1 ndix: B t No:	01/23 of	1
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Loca	ation No):	B8			St	art Date/Time:	10/25/23 1	335	End Date/Time:	1	0/25/23 1345
Con Ope Equ Driv Driv	ducted rator: ipment ⁻ e Weigh e Drop (By: Type: it (lb): in):	J. A A. I CM 140 30	∖lborno Lara IE-75 ŀ)	oz ⊣SA	E) Di Ao Fi	acavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 5' None D3550 None		Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	2 N C D	862 ot Encountered lear riven 4220
Depth (ft)	Description / Comments Light Brown, Dry, Poorly Graded Sand with Silt											Lab Tests (2)
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Con	nments: ountered	"N" Valu durina dri	ie Based o Illing oper	on 2.5" di ations. P	ameter i Partial ca	modified (wina of ho	California Tube Sam le observed.	pler (ASTM D3550)	or SPT (A	STM D1586) as noted	on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansior	ear 1 Index	SA CR	 Sieve Analysis Corrosion 	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
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enco	nments: ountered	"N" Valu durina dr	illina oper	on 2.5" di ations. P	iameter ı Partial ca	modified vina of ho	California Tube Sam ole observed.	ppler (ASTM D3550)	or SPT (/	ASTM D1586) as noted	on log. S	ome boulder/rock
(1)	=Bulk =Driv	en	⁽²⁾ DS EI	=DirectShe =Expansior	ear Index	SA CF	Sieve AnalysisCorrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	> N	Лe	rre	ell,	Jo	hn	son	engine	ering	surveying te	esting	inspection

		ASTM	E 1 D5434,	xplc D1452, [Drat D1586, D	Ory 1587, D2	Log 488 (USCS), D3550)	Repo Sheet Appe Permi	rt Date: 12/0 :: 1 ndix: B it No:	01/23 of	1
Proj Proj Proj Clie	ject Num ject Title ject Loca nt:	iber: : ation:	3813 Indu Appl Redv	3.006. strial E le Valle wood \	500 Buildin ey, CA West	g			Client USA DSA DSA DSA	t Project No: Ticket No: File No: Application No: LEA No:		
Loca	ation No):	B10	C		400	End Date/Time:	1	0/25/23 1405			
Con Ope Equ Driv Driv	nducted erator: ipment ⁻ re Weigh re Drop (By: Type: t (Ib): in):	J. A A. I CM 140 30	∖lborno _ara E-75 ŀ)	oz HSA	E) Di A(Fi Sł	ccavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 5' None D3550 None	1	Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	2: N C D	364 ot Encountered lear riven 4220
Description / Comments Density (pc) (pc) (pc) (pc) (pc) (pc) (pc) (pc)									ients		Lab Tests (2)	
							Drilling Terminat	ed at Approximately	5'			SA, SE, RV
enco	nments: ountered	"N" Valu durina dri	le Based o Ilina oper	on 2.5" di ations. P	iameter Partial ca	modified (vina of ha	California Tube Sam le observed.	npler (ASTM D3550)) or SPT (A	ASTM D1586) as noted o	on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansior	ear Index	SA CR	Sieve AnalysisCorrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	> N	Лe	rre	ell,	Jo	hn	son	engine	ering	surveying te	sting	inspection

		ASTM	E 1 D5434,	xplc D1452, [Drat 01586, D	OľY 1587, D2	Log 488 (USCS), D3550)	Report Sheet: Append Permit I	Date: 12 lix: B No:	2/01/23 1 of	1
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Loca	ation No):	B1 ⁻	1		St	art Date/Time:	10/25/23 1	407	End Date/Time:	1	0/25/23 1410
Con Ope Equ Driv Driv	nducted erator: ipment ⁻ re Weigh re Drop (By: Type: t (Ib): in):	J. A A. I CM 140 30	Alborno Lara IE-75 F	oz HSA	E) Di A(Fi Sł	ccavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 5' None D3550 None	3	Elevation: Groundwater: Recent Weather: Sampler Insertion Preservation:	23 N C D D	867 ot Encountered lear riven 4220
Depth (it) N. Value N. Value N. Value N. Value <td< td=""><td></td><td>Lab Tests (2)</td></td<>											Lab Tests (2)	
							Drilling Terminat	ed at Approximately	5'			SA, SE
enco	nments: ountered	"N" Valu durina dri	illina oper	on 2.5" di ations. P	iameter i Partial ca	modified (vina of ha	California Tube San Ie observed.	npler (ASTM D3550)) or SPT (AS	TM D1586) as note	d on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansior	ear Index	SA	 Sieve Analysis Corrosion 	MD =Max Density RV =R-Value	A	L =Atterberg LimitsE =Sand Equivalent	CN = TD =	Consolidation Tube Density
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		ASTM	E 2 1 D5434, 1	xplc D1452, D)rat 01586, D	Ory 1587, D2	Log 488 (USCS), D3550)	Report Sheet: Appen Permit	t Date: 12/ 1 dix: B No:	/01/23 of	1
Project Number: 3813.006.500 Project Title: Industrial Building Project Location: Apple Valley, CA Client: Redwood West Location No: B12 Start Date/Time: 10/25/23 1416 End Date/Time: 1												
Loca	ation No	:	B12	2		St	art Date/Time:	10/25/23 1	416	End Date/Time:	1(0/25/23 1420
Con Ope Equi Driv Driv	ducted rator: ipment ī e Weigh e Drop (i	Ву: Гуре: t (Ib): in):	J. A A. I CM 140 30	Alborno _ara E-75 H)	oz ISA	E) Di Ai Fi SI	ccavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 5' None D3550 None	9	Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	20 N C D	364 ot Encountered lear riven 4220
Image: Constraint of the state of the st								ents		Lab Tests ⁽²⁾		
							Drilling Terminat	ed at Approximately	5			SA, SE
Com	nments: ountered o	"N" Valu durina dri	ie Based o Illing oper	on 2.5" di ations. P	ameter ı artial ca	modified wina of ha	California Tube Sam ole observed.	npler (ASTM D3550)) or SPT (A	STM D1586) as noted	on log. S	ome boulder/rock
(1)	=Bulk =Drive	'n	⁽²⁾ DS EI	=DirectShe =Expansion	ear Index	SA	 Sieve Analysis Corrosion 	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	Merrell. Johnson engineering surveying testing inspection											

		ASTM	E 1 D5434,	xplc D1452, C	Drat 01586, D	Ory 1587, D2	Log 488 (USCS), D3550		Repo Sheet Appe Permi	rt Date: 12/ : 1 ndix: B t No:	01/23 of	1
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Loca	ation No): 	B13	3		St	art Date/Time:	10/25/23 1	425	End Date/Time:	1	0/25/23 1430
Con Ope Equi Driv Driv	ducted rator: ipment ⁻ e Weigh e Drop (By: Type: nt (Ib): in):	J. A A. I CM 140 30	∖lborno Lara iE-75)	ΟZ	E) Di A(Fi Sł	ccavation Type: imensions: dvance Assist: eld Tests: noring Type:	Auger Hole 8" x 5' None D3550 None	1	Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	23 N C D	862 ot Encountered lear riven 4220
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comm	nents		Lab Tests (2)
	AB - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -										SA, SE	
Com enco	nments: ountered	"N" Valu durina dri	ie Based o Illina oper	on 2.5" di ations. P	iameter i Partial ca	modified (vina of ho	California Tube Sam le observed.	pler (ASTM D3550)) or SPT (A	ASTM D1586) as noted	on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansion	ear 1 Index	SA	Sieve AnalysisCorrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	> N	Лe	rre	əll,	Jo	hn	son	engine	ering	surveying te	esting	inspection

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		ASTM	E 2 1 D5434, 1	xplc D1452, C)rat (Ory 1587, D2	Log 488 (USCS), D3550		Report I Sheet: Append Permit N	Date: 12 1 ix: B lo:	/01/23 of	1
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Loca	ation No	o: B14	1 Dachs	shund /	Avenue	e St	art Date/Time:	10/25/23 1	425	End Date/Time:	1(0/25/23 1430
Con Ope Equi Driv Driv	ducted rator: ipment ⁻ e Weigh e Drop (By: Type: t (lb): in):	J. A A. I CM 14(30	Alborno Lara IE-75)	ĴΖ	E) Di A(Sł	xcavation Type: imensions: dvance Assist: eld Tests: horing Type:	Auger Hole 8" x 5' None D3550 None		Elevation: Groundwater: Recent Weather: Sampler Insertion: Preservation:	28 N C C D	362 ot Encountered lear riven 4220
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Commen	ts		Lab Tests ⁽²⁾
							Drilling Terminate	ed at Approximately	5'			SA, SE
Con	nments: ountered o	"N" Valu durina dri	e Based o Ilina oper	on 2.5" di ations. P	ameter n 'artial cav	modified (vina of ho	California Tube Sam ole observed.	pler (ASTM D3550)	or SPT (AS	TM D1586) as noted	d on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansion	ear I I ndex	SA	Sieve AnalysisCorrosion	MD =Max Density RV =R-Value	AL	 = Atterberg Limits = Sand Equivalent 	CN = TD =	Consolidation Tube Density
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		ASTM	E 1 D5434, 1	xplc D1452, D)rat 01586, D	Ory 1587, D2	Log 488 (USCS), D3550		Report Sheet: Appen Permit	t Date: 12 1 dix: B No:	/01/23 of	1
Proj Proj Proj Clie	ect Num ect Title ect Loca nt:	iber: : ation:	3813 Indu Appl Redv	3.006. strial E le Valle wood \	500 }uilding əy, CA West	3			Client USA T DSA F DSA A DSA L	Project No: icket No: ile No: pplication No: EA No:		
Loc	ation No): B1	5, Card	ova Ro	bad	St	art Date/Time:	10/25/23 1	425	End Date/Time:	1	0/25/23 1430
Conducted By: Operator:J. AlbornozExcavation Type: Dimensions:Auger Hole 8" x 5'Elevation: Groundwater:2862 Not EncouEquipment Type:CME-75Advance Assist:NoneRecent Weather: Dive Weight (lb):CME-75Advance Assist:NoneRecent Weather: DivenClear Drive Drop (in):Drive Drop (in):30Shoring Type:NonePreservation:D4220						862 ot Encountered lear riven 4220						
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comme	ents		Lab Tests ⁽²⁾
							Drilling Terminate	d at Approximately	5'			SA, SE
Con	nments: ountered	"N" Valu durina dri	ie Based o Illina oper	on 2.5" di ations. P	ameter r 'artial ca	modified (vina of ha	California Tube Samp ole observed.	bler (ASTM D3550)	or SPT (A	STM D1586) as noted	l on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansion	ear NIndex	SA	 Sieve Analysis Corrosion 	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	> N	Ле	rre	ell.	Jo	hn	son	engine	ering	surveying te	esting	inspection

		ASTM	E 1 D5434,	xplc D1452, C)rat	Ory 1587, D2	Log 488 (USCS), D3550		Report Sheet: Appen Permit	t Date: 12 1 dix: B No:	/01/23 of	1
Proj Proj Proj Clie	ect Num ect Title ect Loca nt:	iber: : ation:	3813 Indu Appl Redv	3.006. strial E le Valle wood \	500 3uilding əy, CA West	3			Client USA T DSA F DSA A DSA L	Project No: icket No: ile No: pplication No: EA No:		
Loc	ation No): B1	6, Carc	lova Ro	oad	St	art Date/Time:	10/25/23 1	425	End Date/Time:	1	0/25/23 1430
Conducted By:J. AlbornozExcavation Type:Auger HoleElevation:2862Operator:A. LaraDimensions:8" x 5'Groundwater:Not EncodeEquipment Type:CME-75Advance Assist:NoneRecent Weather:ClearDrive Weight (lb):140Field Tests:D3550Sampler Insertion:DrivenDrive Drop (in):30Shoring Type:NonePreservation:D4220						862 ot Encountered lear riven 4220						
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Comme	ents		Lab Tests ⁽²⁾
							Drilling Terminate	d at Approximately	5'			SA, SE
Con	nments: ountered	"N" Valu durina dri	ie Based o Illing oper	on 2.5" di ations. P	ameter r 'artial ca	modified (vina of ha	California Tube Samı ole observed.	bler (ASTM D3550)	or SPT (A	STM D1586) as noted	l on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansion	≥ar iIndex	SA	Sieve AnalysisCorrosion	MD =Max Density RV =R-Value		AL =Atterberg Limits SE =Sand Equivalent	CN = TD =	Consolidation Tube Density
	> N	Ле	rre	ell.	Jo	hn	son	engine	ering	surveying te	esting	inspection

		ASTM	E 2 1 D5434, 1	xplc D1452, D)rat()1586, D	Ory 1587, D2	Log 488 (USCS), D3550		Report Sheet: Append Permit I	Date: 12/ 1 lix: B No:	/01/23 of	1
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Loca	ation No	9: B17	, Dach	shund	Avenue	e St	art Date/Time:	10/25/23 1	425	End Date/Time:	1()/25/23 1430
Conducted By:J. AlbornozExcavation Type:Auger HoleElevation:2862Operator:A. LaraDimensions:8" x 5'Groundwater:Not EnEquipment Type:CME-75Advance Assist:NoneRecent Weather:ClearDrive Weight (lb):140Field Tests:D3550Sampler Insertion:DrivenDrive Drop (in):30Shoring Type:NonePreservation:D4220						362 ot Encountered ear riven 4220						
Depth (ft)	'N' Value	Sample ⁽¹⁾	Moisture (%)	Density (pcf)	Class (USCS)	Graphic		Descriptio	n / Commei	nts		Lab Tests (2)
							Drilling Terminate	o 5' - JDA10252328	5			SA, SE
Con	nments: ountered o	"N" Valu durina dri	e Based o Ilina oper	on 2.5" di ations. P	ameter n 'artial cav	modified vina of ho	California Tube Sam ble observed.	pler (ASTM D3550)) or SPT (AS	TM D1586) as noted	on log. S	ome boulder/rock
(1)	=Bulk =Drive	en	⁽²⁾ DS EI	=DirectShe =Expansion	ear Index	SA	 Sieve Analysis Corrosion 	MD =Max Density RV =R-Value	A	L =Atterberg Limits E =Sand Equivalent	CN = TD =	Consolidation Tube Density
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APPENDIX C

Laboratory Testing

































Laboratory Com	paction Characteris	stics	Report Date: Sheet: Attachment: Permit No.:	12/0 1 c	1/23 of 1	
Project Number:3813.006Project Title:IndustrialProject Location:Apple ValClient:Redwood	.600 Building ley, CA West		Client Project No.: Other: DSA File No.: DSA Application N DSA LEA No.:	: No.:		
Sample ID: JDA10252301	Maximum Dry Unit Weight (lbf/ft ³)	: 124.1	Optimum Mois	sture Content (%	6) : (9.2
Classification, ASTM D2488: (Sample Origin: B Laboratory Remarks:	SM) Silty sand oring One at 0' to 5'					
150 145 140			Tested By: Received Mois Preparation: Specific Gravit SG Method:	ture: y:	DRS 3.8% Wet	2 0
135 130 125 120 115			Start Weight (II Retained on 3/ Retained on 3/ Retained on N Retained on 3/ Retained on 3/ Retained on N Oversize Corre	b): 4" (lb): 8" (lb): 0. 4 (lb): 4" (%): 8" (%): 0. 4 (%): ection :	35.0 0.2 0.7 1.9 0.6% 2.0% 5.4%) ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
110 105 100			Mold Volume F Tare Weight (lb Rammer Used:	Factor:): :	29.9 4.35 Mechan	4 5 lical
0% 5% 10'	% 15% 20%	25%	30% Method Used:	A	, / В	С
Weight of Soil and Tare (b): Wet Weight (g): Dry Weight (g): Moisture Content (%): Dry Unit Weight (flb/ft ³):	8.64 349.4 330.4 5.8% 121.5	8.81 311.7 288.8 7.9% 123.7	8.89 373.1 339.8 9.8% 123.8		8.79 347.5 310.9 11.8% 118.9	
The Material Was The Material Tested Met cc: Project Architect, Structural Engineer	Was Not Sampled & t Did Not Meet The requirer , Project Inspector, DSA Regional Office,	ested in accordance ments of the DSA a School District	ce with the reqs. of the D approved documents.	SA approved doc	uments.	
Reviewed By	(Signature)	J	eremy Beissner / I _{Nam}	_aboratory N e / Title	lanager	
	ISON	Dncept t	co complet			ECTION

Laboratory Com	paction Cha	aracteristic	S	Report Date: Sheet: Attachment: Permit No.:	12/01/2 1 of C	23 1	
Project Number:3813.006Project Title:IndustrialProject Location:Apple VaClient:Redwood	5.600 Building Illey, CA I West			Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:			
Sample ID: JDA10252310	Maximum Dry Uni	it Weight (lbf/ft ³):	126.5	Optimum Moisture C	ontent (%):	ç	9.4
Classification, ASTM D2488: (Sample Origin: Laboratory Remarks:	SPSM) Poorly grad Boring Two at 5' to	ed sand with silt 10'					
150 145 140				Tested By: Received Moisture: Preparation: Specific Gravity: SG Method:		DRS 3.6% Wet	0
135 130 125 120 115				Start Weight (b): Retained on 3/4" (b): Retained on 3/8" (b): Retained on No. 4 (b): Retained on 3/4" (%): Retained on 3/8" (%): Retained on No. 4 (%) Oversize Correction:	:	35.0 0.0 0.2 1.4 0.6% 4.0%) 0 0
				Mold Volume Factor: Tare Weight (b): Rammer Used:		29.94 4.35 Mechan	4 ical
0% 5% 10	% 15%	20% 25	%	^{30%} Method Used:	., A	В	С
Weight of Soil and Tare (b): Wet Weight (g): Dry Weight (g): Moisture Content (%): Dry Unit Weight (fb/ft ⁸):	8.69 323.0 307.1 5.2% 123.5	8. 32 29 7. 12	86 1.2 9.9 1% 6.1	8.94 317.1 290.4 9.2% 125.9		8.79 339.4 305.4 11.1% 119.6	
The Material Was The Material Tested Met cc: Project Architect, Structural Enginee	Was Not Did Not Meet r, Project Inspector, DSA I	Sampled & tested The requirements Regional Office, Schoo	in accordance of the DSA ap ol District	e with the reqs. of the DSA app oproved documents.	roved docum	nents.	
Reviewed B	D assurz vy (Signature)		Je	remy Beissner / Labor _{Name / Title}	atory Ma	nager	
	nson		cept to	O COMPLETION	ESTING	INSP	ECTION
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Laboratory Com	paction Chara	acteristics		Report Date: Sheet: Attachment: Permit No.:	12/01/23 1 of C	3 1	
Project Number:3813.000Project Title:IndustrialProject Location:Apple VaClient:Redwood	5.600 Building Illey, CA I West			Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:			
Sample ID: JDA10252311	Maximum Dry Unit W	/eight (lbf/ft ³):	122.5	Optimum Moisture Co	ontent (%):	ç	1.1
Classification, ASTM D2488: (Sample Origin: E Laboratory Remarks:	SPSM) Poorly graded 3oring Three at 0' to 5	l sand with silt 5'					
150 145 140				Tested By: Received Moisture: Preparation: Specific Gravity: SG Method:		DRS 3.4% Wet)
135 130 125 120 115				Start Weight (b): Retained on 3/4" (b): Retained on 3/8" (b): Retained on No. 4 (b): Retained on 3/4" (%): Retained on 3/8" (%): Retained on No. 4 (%): Oversize Correction:		25.0 0.3 1.1 2.6 1.2% 4.4% 10.4%)) 6
				Mold Volume Factor: Tare Weight (Խ): Rammer Used:	I	29.94 4.35 Mechan	1 ical
0% 5% 10	% 15%	20% 25%	30	[%] Method Used:	A	. / В	С
Weight of Soil and Tare (b): Wet Weight (g): Dry Weight (g): Moisture Content (%): Dry Unit Weight (fb/ft ³):	8.56 349.4 331.6 5.4% 119.6	8.71 320.8 298.6 7.4% 121.5	5	8.82 332.2 303.5 9.5% 122.3		8.79 321.8 289.1 11.3% 119.4	
The Material Was The Material Tested Met cc: Project Architect, Structural Enginee	Was Not Did Not Meet r, Project Inspector, DSA Reg	Sampled & tested in ac The requirements of th gional Office, School Di	ccordance v le DSA app strict	vith the reqs. of the DSA appr roved documents.	oved docume	ents.	
Reviewed B	y (Signature)		Jere	emy Beissner / Labora _{Name / Title}	atory Man	nager	
	nson	CONCE ENGINEEF	pt to	SURVEYING TE	STING		ECTION

Laboratory Com	Daction Characteris	stics	Report Date: Sheet: Attachment: Permit No.:	12/01/23 1 of 1 C
Project Number:3813.006Project Title:IndustrialProject Location:Apple ValClient:Redwood	.600 Building ley, CA West		Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:	
Sample ID: JDA10252315	Maximum Dry Unit Weight (\bf/ft ³):	128.1	Optimum Moisture	Content (%): 6.5
Classification, ASTM D2488: (S Sample Origin: B Laboratory Remarks:	SM) Silty sand oring Four at 0' to 5'			
150 145 140			Tested By: Received Moisture: Preparation: Specific Gravity: SG Method:	DRS 3.6% Wet
135 130 125 120 115			Start Weight (b): Retained on 3/4" (b): Retained on 3/8" (b): Retained on No. 4 (b) Retained on 3/4" (%): Retained on 3/8" (%): Retained on No. 4 (%) Oversize Correction	31.0 0.4 0.8 0: 1.6 : 1.3% : 2.6% 6): 5.2%
110			Mold Volume Factor Tare Weight (b): Rammer Used:	r: 29.94 4.35 Mechanical
0% 5% 104	% 15% 20%	25%	^{30%} Method Used:	□А √В □С
Weight of Soil and Tare ((b): Wet Weight (g): Dry Weight (g): Moisture Content (%): Dry Unit Weight (flb/ft ³):	8.60 323.7 312.5 3.6% 122.8	8.85 308.2 292.0 5.5% 127.6	8.94 318.4 296.0 7.6% 127.8	8.89 343.2 313.0 9.6% 124.0
The Material Was The Material Tested Met cc: Project Architect, Structural Engineer	Was Not Sampled & te Did Not Meet The requiren , Project Inspector, DSA Regional Office, S	ested in accordance nents of the DSA a School District	ce with the reqs. of the DSA ap approved documents.	proved documents.
Reviewed By	(Signature)	J	eremy Beissner / Labo Name / Title	pratory Manager
	ISON CC	ncept t	Co completion	

Sand Equivalent	of Soils and Fine Aggi ASTM D2419	regate Report I Sheet: Attachm Permit N	Date: 12/C 1 nent: No.:	01/23 of 1 C
Project Number:3813.0Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA pod West	Client P Other: DSA File DSA Ap DSA LE	roject No.: e No.: plication No.: A No.:	
Sample ID: JDA10252323	General Compliance	Non-Complian	ce	Not Specified
Desription: Sample Origin: Laboratory Remarks:	(SPSM) Poorly graded sand w Boring Eight at 0' to 5'	vith silt		
Tested By: Mechanical/Manual Shaker:	JJB Mechanical			
	Sand Equivalent Value	Ammount/	Value Allowable	
	71		-	
Ammount/Value Allowable Bas	ed On:			
The Material V The Material Tested N cc: Project Architect, Structural Engi	Vas Was Not Sampled & 1et Did Not Meet The requir neer, Project Inspector, DSA Regional Offic	& tested in accordance with the rea rements of the DSA approved docu e, School District	qs. of the DSA approved o uments.	documents.
Review	ied By (Signature)	Jeremy Be	issner/ Laboratory Name / Title	Manager
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Sand Equivalent	of Soils and Fine Aggi ASTM D2419	Report Date: Sheet: Attachment: Permit No.:	12/01/23 1 of 1 C	
Project Number:3813.0Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA rod West		Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:	
Sample ID: JDA10252324	General Compliance	No	n-Compliance	Not Specified
Desription: Sample Origin: Laboratory Remarks:	(SM) Silty sand with Boring Nine at 0' to 5'			
Tested By: Mechanical/Manual Shaker:	JJB Mechanical			
	Sand Equivalent Value		Ammount/Value Allowable	e
	36			
Ammount/Value Allowable Bas	ed On:			
The Material W The Material Tested M cc: Project Architect, Structural Engi	/as Was Not Sampled & let Did Not Meet The requir neer, Project Inspector, DSA Regional Offic	& tested in accordance rements of the DSA a re, School District	ce with the reqs. of the DSA a approved documents.	oproved documents.
			eremy Beissner/ Labo	pratory Manager
Review	ed By (Signature)		Name / Titl	8
	nnson	concept t	co completion	n Testing Inspection
MEC-108 SE 09/15			t)760.25	i6.2068 f)760.256.0418 w)www.merrelljohnson.com

Sand Equivalent	of Soils and Fine Aggreen ASTM D2419	egate Report Sheet: Attach Permit	t Date: 12/01/2 1 of No.: C	13 1
Project Number:3813.0Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA pod West	Client Other: DSA F DSA A DSA L	Project No.: ile No.: pplication No.: EA No.:	
Sample ID: JDA10252325	General Compliance	Non-Complia	ince Not	Specified
Desription: Sample Origin: Laboratory Remarks:	(SM) Silty sand with gravel Boring Ten at 0' to 5'			
Tested By: Mechanical/Manual Shaker:	JJB Mechanical			
	Sand Equivalent Value	Ammoun	t/Value Allowable	
	24		-	
Ammount/Value Allowable Bas	ed On:			
The Material V The Material Tested N cc: Project Architect, Structural Engi	Vas Was Not Sampled & Net Did Not Meet The require neer, Project Inspector, DSA Regional Office	tested in accordance with the r ements of the DSA approved do a, School District	eqs. of the DSA approved docum cuments.	ients.
Review	red By (Signature)	Jeremy B	eissner/ Laboratory Mar Name / Title	nager
Merrelljor	nnson er	ONCEPT TO CON	mpletion	INSPECTION
MEC-108 SE 09/15			t)760.256.2068 f)760.256.0	0418 w)www.merrelljohnson.com

Sand Equivalent	of Soils and Fine Aggr ASTM D2419	egate Re Sh At Pe	eport Date: leet: tachment: rrmit No.:	12/01/23 1 of 1 C
Project Number:3813.(Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA pod West		ient Project No.: .her: SA File No.: SA Application No.: SA LEA No.:	
Sample ID: JDA10252326	General Compliance	Non-Com	npliance	Not Specified
Desription: Sample Origin: Laboratory Remarks:	(SM) Silty sand with gravel Boring Eleven at 0' to 5'			
Tested By: Mechanical/Manual Shaker:	JJB Mechanical			
	Sand Equivalent Value	Amm	ount/Value Allowable	
	24			
Ammount/Value Allowable Bas	ed On:			
The Material	Vas Was Not Sampled & let Did Not Meet The require neer, Project Inspector, DSA Regional Office	a tested in accordance with ements of the DSA approve e, School District	the reqs. of the DSA app ad documents.	proved documents.
		lerem	v Beissner/ Labo	ratory Manager
Review	ed By (Signature)		Name / Title	
		an actual d		
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MEC-108 SE 09/15			t)760.256	.2068 f)760.256.0418 w)www.merrelljohnson.com

Sand Equivalent	of Soils and Fine Agg	Report Date: 12/01/23 Sheet: 1 of 1 Attachment: C Permit No.: C			
Project Number:3813.0Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA ood West		Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:		
Sample ID: JDA10252327	General Compliance	No	n-Compliance	Not Specified	
Desription: Sample Origin: Laboratory Remarks:	(SM) Silty sand Boring Twelve at 0' to 5'				
Tested By: Mechanical/Manual Shaker:	JJB Mechanical				
	Sand Equivalent Value		Ammount/Value Allowable		
	17		-		
Ammount/Value Allowable Bas	ed On:				
The Material W The Material Tested M cc: Project Architect, Structural Engi	Vas Was Not Sampled Iet Did Not Meet The requi neer, Project Inspector, DSA Regional Offic	& tested in accordanc rements of the DSA a ce, School District	e with the reqs. of the DSA approved documents.	proved documents.	
		J	eremy Beissner/ Labo	ratory Manager	
Review	ed By (Signature)		Name / Title	2 - 0 -	
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Sand Equivalent	of Soils and Fine Aggi ASTM D2419	Report Date:12/01/23Sheet:1Attachment:CPermit No.:C					
Project Number:3813.0Project Title:IndustProject Location:AppleClient:Redword	006.500 rial Building Valley, CA pod West		Client Project No.: Other: DSA File No.: DSA Application No.: DSA LEA No.:				
Sample ID: JDA10252328	General Compliance	No	n-Compliance	Not Specified			
Desription: Sample Origin: Laboratory Remarks:	(SM) Silty sand with Boring Thirteen at 0' to 5'						
Tested By: Mechanical/Manual Shaker:	JJB Mechanical						
	Sand Equivalent Value		Ammount/Value Allowabl	e			
	37						
Ammount/Value Allowable Bas	ed On:						
The Material V The Material Tested N cc: Project Architect, Structural Engi	Vas Was Not Sampled & Iet Did Not Meet The requir neer, Project Inspector, DSA Regional Offic	& tested in accordanc rements of the DSA a ce, School District	ce with the reqs. of the DSA approved documents.	pproved documents.			
		J	eremy Beissner/ Labo	pratory Manager			
Review	ed By (Signature)		Name / Titl	e			
	nnson	concept t	co completion	n Testing Inspection			
MEC-108 SE 09/15			t)760.25	6.2068 f)760.256.0418 w)www.merrelljohnson.com			



12/23

(ASTM D2435)

R-Value Project Numb Project Title: Project Locat Client:	e and Expans	ASTM D2844 ASTM D2844 006.600 ial Building Valley, CA od West	Report Date: Sheet: Appendix: Permit No.: Client Project I Other: DSA File No.: DSA Applicatio DSA LEA No.:	12/01 1 of C No.: on No.:	/23	
Sample ID:	JDA10252325	General Complian	ce No	on-Compliance	No	t Specified
Desription, D Sample Origin Tested By:	2847: n:	(SM) Silty sand with gra Boring Ten at 0' to 5' , JJB	avel East Side of Warehous	se		
		Briguette Number: Moisture Content (%): Dry Density (pcf): Exudation Pressure (psi): Expansion Pressure (psf): R-Value: R-Value &	1 12.9 124.4 756 0 30 Expansion VS. Ex	2 15.1 118.9 456 0 28 udation	3 14.8 128.6 254 0 24	
100 95 90 85 80 75 70 65 60 91 55		F	R-Value at 300 psi = 25			
40 40 35 30 25 20 15 10		24	28			30
5 0 0	100	200 300	400 Expansion Pressure, psi	500	600 7	700 800
The Material The Material cc: Project Arc	Tested M Shitect, Structural Engin	Vas Was Not S et Did Not Meet neer, Project Inspector, DSA Regi	Sampled & tested in accordance The requirements of the DSA a onal Office, School District	ce with the reqs. of th approved documents	e DSA approved docu	ments.
	Review	Builder ed By (Signature)	J	Jeremy Beissne	r / Laboratory Mana / Title	anager
		nnson	concept 1 ENGINEERING	to comple		

R-Value and Expansion Pressure of Compacted Soils ASTM D2844 Project Number: 3813.006.600 Project Title: Industrial Building Project Location: Apple Valley, CA Client: Redwood West					Report Date:12/01/23Sheet:1of1Appendix:CCPermit No.:CClient Project No.:COther:DSA File No.:DSA Application No.:DSA LEA No.:			
Sample ID:	JDA10252327	Gener	ral Compliance	No	on-Compliance		Not Specified	
Desription, D Sample Origi Tested By:	02847: n:	(SM) Silty sai Boring Twelv JJB	nd e at 0' to 5', West	Side of Wareh	nouse			
	E	Briguette Nur Moisture Conte Dry Density (ixudation Pressu xpansion Pressu R-Value: R	nber: nt (%): pcf): ıre (psi): ıre (psf): Value & Expan	1 10.7 126.3 725 0 22 sion VS. Ex	2 11.8 125.6 412 0 19	3 15.8 112.4 151 0 14		
100 95 90			R-Value :	at 300 psi = 17				
80 75 70 65 60 55 50 								
30 25 20	14			19			22	
15 10 5								
0	100	200	300 Expans	400 ion Pressure, psi	500	600	700 800	
The Material The Material cc: Project Arc	Tested Met	Was N Did N er, Project Inspec	Not Sampled 8 of Meet The requir tor, DSA Regional Office	tested in accordan ements of the DSA e, School District	ice with the reqs. of th approved documents	e DSA approved (documents.	
	Reviewed	By (Signature)			Jeremy Beissne	r / Laborator	y Manager	
		nsor	C		to comple			

R-Value Project Numbe Project Title: Project Locatio Client:	Report Date: Sheet: Appendix: Permit No.: Client Project Other: DSA File No.: DSA Applicat DSA LEA No.	1: 1 C No.: ion No.: :	2/01/23 of 1					
Sample ID:	JDA11292302	Gener	ral Compliance	No	on-Compliance		Not Specified	
Desription, D28 Sample Origin: Tested By:	347:	(SM) Silty sai Boring Fourte JJB	nd een at 0' to 5' , [Dachund Avenue)			
	E	Briguette Nur Moisture Conte Dry Density (ixudation Pressu xpansion Pressu R-Value: R-V	nber: nt (%): pcf): ire (psi): ire (psf): Value & Expa	1 7.0 129.1 741 0.0135 60 nsion VS. Ex	2 7.5 130.9 397 0.0169 61 udation	3 9.1 127.9 143 0.0194 52		
100 95 90			R-Value	at 300 psi = 58				
85 80 75 70 65 60 90 55 50 40 40 40 35 30 25 25	52			61			60	
15 10 5 0 0	100	200	300 Expar	400 nsion Pressure, psi	500	600	700	800
The Material The Material Te cc: Project Archi	ested Was Met tect, Structural Engine	Was N Did No er, Project Inspect	Not Sampled ot Meet The requ tor, DSA Regional Offi	& tested in accordan irements of the DSA ce, School District	ce with the reqs. of t approved document	he DSA approve s.	ed documents.	
	Reviewed	Beimer By (Signature)			Jeremy Beissn	er / Laborat Name / Title	ory Manager	
		nsor	1		to compl		TING INSP	ECTION

R-Value and Project Number: Project Title: Project Location: Client:	Report Date: Sheet: Appendix: Permit No.: Client Project Other: DSA File No.: DSA Applicati DSA LEA No.:	1 C No.: on No.:	of 1				
Sample ID: JDA11	1292303 Genera	l Compliance	No	n-Compliance	[Not Specified	
Desription, D2847: Sample Origin: Tested By:	(SM) Silty san Boring Fifteer JJB	d i at 0' to 5' Cardo	ova Avenue				
	Briguette Num Moisture Conten Dry Density (p Exudation Pressur Expansion Pressur R-Value: R-V	ber: t (%): cf): e (psi): e (psf): alue & Expans	1 7.5 129.9 699 0.0031 64 sion VS. Ext	2 8.1 130.5 469 0.0017 58 udation	3 8.8 127.8 188 0.0008 48		
100 95 90		R-Value a	t 300 psi = 52				
80 75 70 65 60 90 100 55 50 70 65 60 80 75 70 65 60 80 75 70 65 60 80 75 70 65 80 70 65 80 75 70 65 80 80 80 80 80 80 80 80 80 80 80 80 80	48		58	3		64	
25 20 15 10 5 0 0	100 200	300 Expansio	400 on Pressure, psi	500	600	700	800
The Material The Material Tested cc: Project Architect, Str	Was Was No Met Did No ructural Engineer, Project Inspecto	ot Sampled & t Meet The required r, DSA Regional Office,	tested in accordance ments of the DSA a School District	ce with the reqs. of the approved documents	ne DSA approved.	d documents.	
	Reviewed By (Signature)		J	leremy Beissne	er / Laborato	ory Manager	
	Johnson	CC EN	oncept t	co compl	etion G TEST	ING INSF	




Project Number: 3813.006.500 Project Title: Industrial Building Project Location: Apple Valley, CA Client: Redwood West		Report Date:12/01/23Sheet:1of1Attachment:CPermit No.:CClient Project No.:COther:DSA File No.:DSA Application No.:DSA LEA No.:				
Sample ID: JDA10252311	General Compliance	No	on-Compliance Not Specified			
Classification, ASTM D2487: Sample Origin: Laboratory Remarks:	(SPSM) Poorly graded sand wit Boring Three at 0' to 5'	th silt				
Tested By: Method/Procedure:	JJB ASTM D4829					
Expansion Index						
	value.	. Ζ				
	Expansion Index	Pot	tention Expansion			
0 - 20		Very Low				
21 - 50		Low				
51 - 90		Medium				
91 - 130		High				
	> 130		Very High			
The Material Was Was Not Sampled & tested in accordance with the reqs. of the DSA approved documents. The Material Tested Met Did Not Meet The requirements of the DSA approved documents. cc: Project Architect, Structural Engineer, Project Inspector, DSA Regional Office, School District School District						
Reviewe	By (Signature)	J	leremy Beissner / Laboratory Manager Name / Title			
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Project Number: Project Title: Project Location: Client: Broject Number: Project Number: Project Number: Project Number: Redwood West	n Potential 22, 417, 643	Report Date: 12/01/23 Sheet: 1 of 1 Appendix: C Permit No: C Client Project No: Other: DSA File No: DSA File No: DSA LEA No: DSA LEA No:		
Sample ID: JDA10252310				
Classification, ASTM D2487: (SPSM Sample Origin: Boring Laboratory Remarks:) Poorly graded sand with Two at 5' to 10'	silt		
Analysis	Result	Units	Test Method	
Minimum Resistivity	1,500	ohm-cm	CT 643	
Chloride Content	260	ppm	CT 422	
Sulfate Content	0.006	%	CT 417	
The Material Tested Was The Material Tested Met cc: Project Architect, Structural Engineer, Pro	Was Not Sampled & te Did Not Meet The requirem ject Inspector, DSA Regional Office.	sted in accordance with the reqs. of ents of the DSA approved documer , School District Jeremy Beiss	the DSA approved documents. tts. ner/ Laboratory Manager	
Reviewd By (Signature	ohnson.	engineering surv	Name / Title	

Project Number: Project Title: Project Location: Client: Broject Location: Client: Broject Location: Client: Broject Number: Project Number: P	n Potential 22, 417, 643 ing CA	Report Date: Sheet: Appendix: Permit No: Client Project Other: DSA File No: DSA Applicat DSA LEA No:	Report Date: 12/01/23 Sheet: 1 of 1 Appendix: C Permit No: C Client Project No: Other: DSA File No: DSA Application No: DSA LEA No: DSA LEA No:		
Sample ID: JDA10252311					
Classification, ASTM D2487: (SPSM Sample Origin: Boring Laboratory Remarks:) Poorly graded sand with Three at 0' to 5'	silt			
Analysis	Result	Units	Test Method		
Minimum Resistivity	260	ohm-cm	CT 643		
Chloride Content	1230	ppm	CT 422		
Sulfate Content	0.177	%	CT 417		
The Material Was The Material Tested Met cc: Project Architect, Structural Engineer, Pro	Was Not Sampled & te Did Not Meet The requiren ject Inspector, DSA Regional Office	ested in accordance with the reqs. of nents of the DSA approved documen a, School District	the DSA approved documents. ts.		
Reviewd By (Signature)	Jeremy Beiss	ner/ Laboratory Manager		
Merrell Jo	ohnson.	engineering surv	eying testing inspection		

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